

# SECOND QUARTERLY AMBIENT AIR MONITORING REPORT LIVINGSTON RAIL YARD

Submitted to:

# Montana Department of Health and Environmental Sciences

Cogswell Building Helena, Montana 59620

STATE DOCUMENTS COLLECTION

JAN 7 1992

Prepared by:

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Submittal Date: June 7, 1991

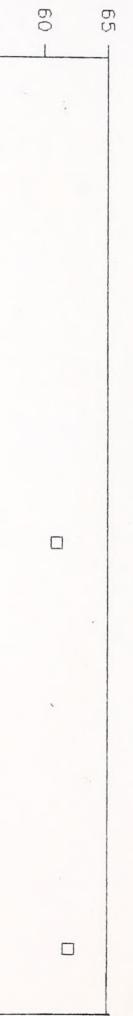
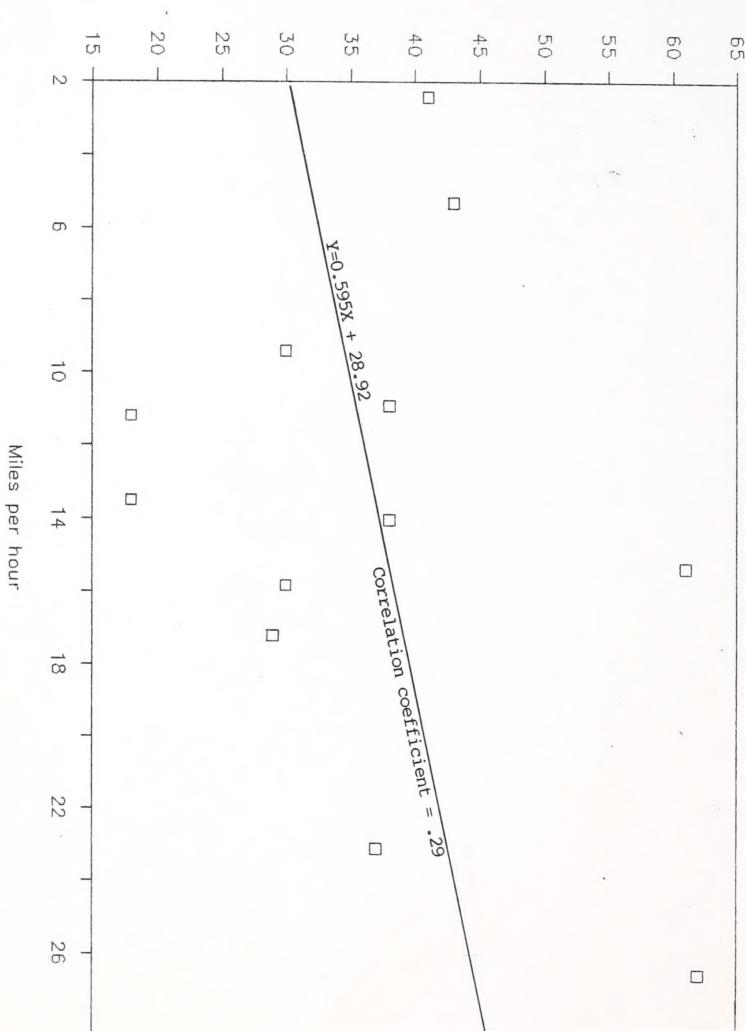


FIGURE 6.0 - SECOND QUARTERLY AMBIENT AIR MONITORING REPORT

TSP VS WIND SPEED

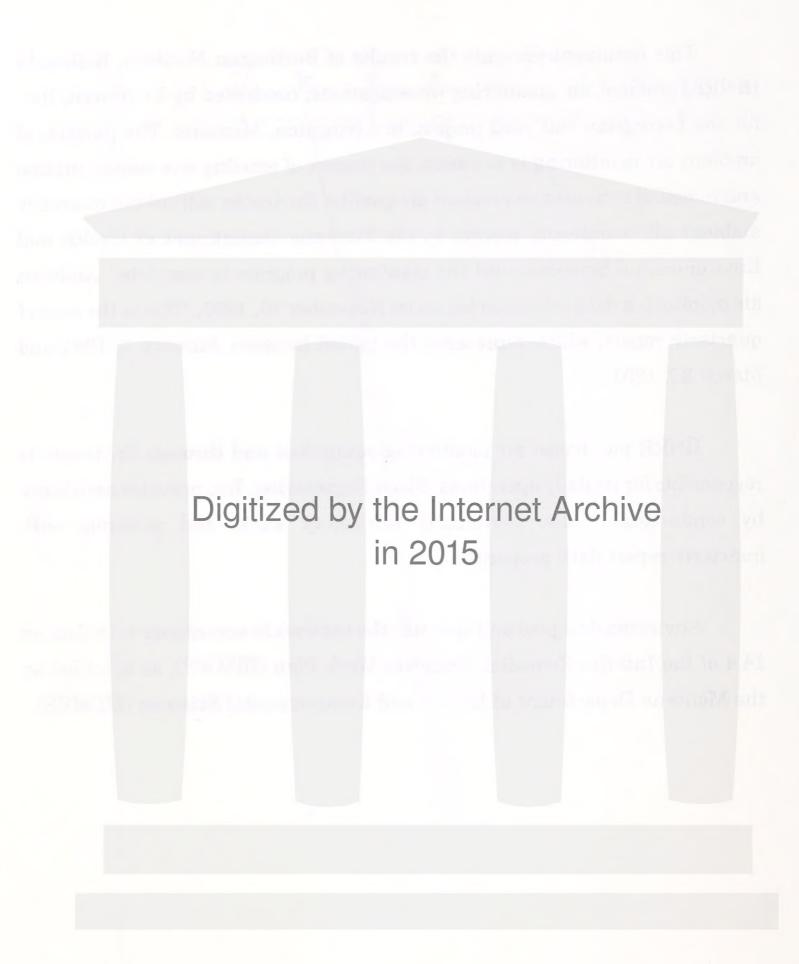


#### 1.0 INTRODUCTION

This document presents the results of Burlington Northern Railroad's (BNRR) ambient air monitoring investigations, conducted by Envirocon, Inc., for the Livingston rail yard project, in Livingston, Montana. The purpose of ambient air monitoring is to assess the impact of existing site contamination and remedial activities on ambient air quality. Envirocon will submit quarterly ambient air monitoring reports to the Montana Department of Health and Environmental Sciences until the monitoring program is complete. Ambient air monitoring data collection began on November 10, 1990. This is the second quarterly report, which represents the period between January 1, 1991 and March 31, 1991.

BNRR purchased air monitoring equipment and through Envirocon is responsible for its daily operations. Bison Engineering, Inc. provides assistance by conducting audits, performing laboratory work, and assisting with quarterly-report data preparation.

Envirocon designed and operates the network in accordance with Section 14.4 of the Interim Remedial Measures Work Plan (IRMWP), as specified by the Montana Department of Health and Environmental Sciences (MDHES).



#### 2.0 NETWORK CONFIGURATION

#### 2.1 Monitoring Locations - General

Envirocon established an ambient air monitoring network near the Livingston rail yard to measure upwind and downwind air quality during remedial activities. Requirements for this network are outlined in Section 14.4 of the IRMWP. The network consists of an upwind station (Station No. 1) and a downwind station (Station No. 2). Each station contains a PM-10 air monitoring instrument. Station No. 2 also contains meteorological equipment, a total suspended particulate (TSP) sampler, and a polyurethane foam (PUF) sampler (presently not in use) designed to measure polynuclear aromatic hydrocarbons (PNAs). PUF sampling and metal measurements were only required during the first six sampling events of the first quarter.

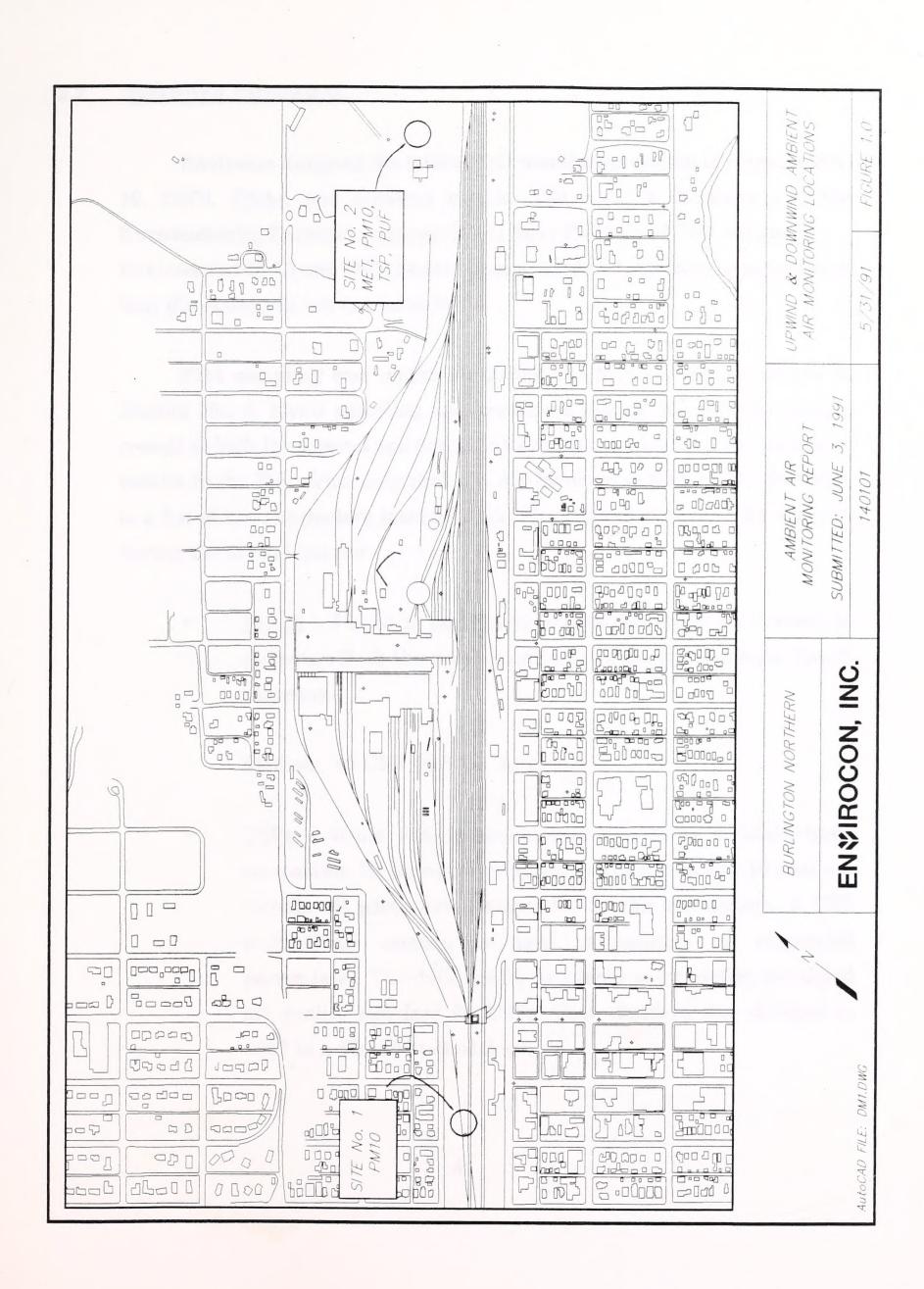
Station No. 1 measures ambient air quality upwind of all remedial activities. Station No. 2 is located to measure worst-case ambient air impacted by remediation activities. In addition, ambient air at Station No. 2 is impacted by current railyard operations. Figure 1.0 shows the locations of both stations. The coordinate locations of these sites are shown on Table 1.0.

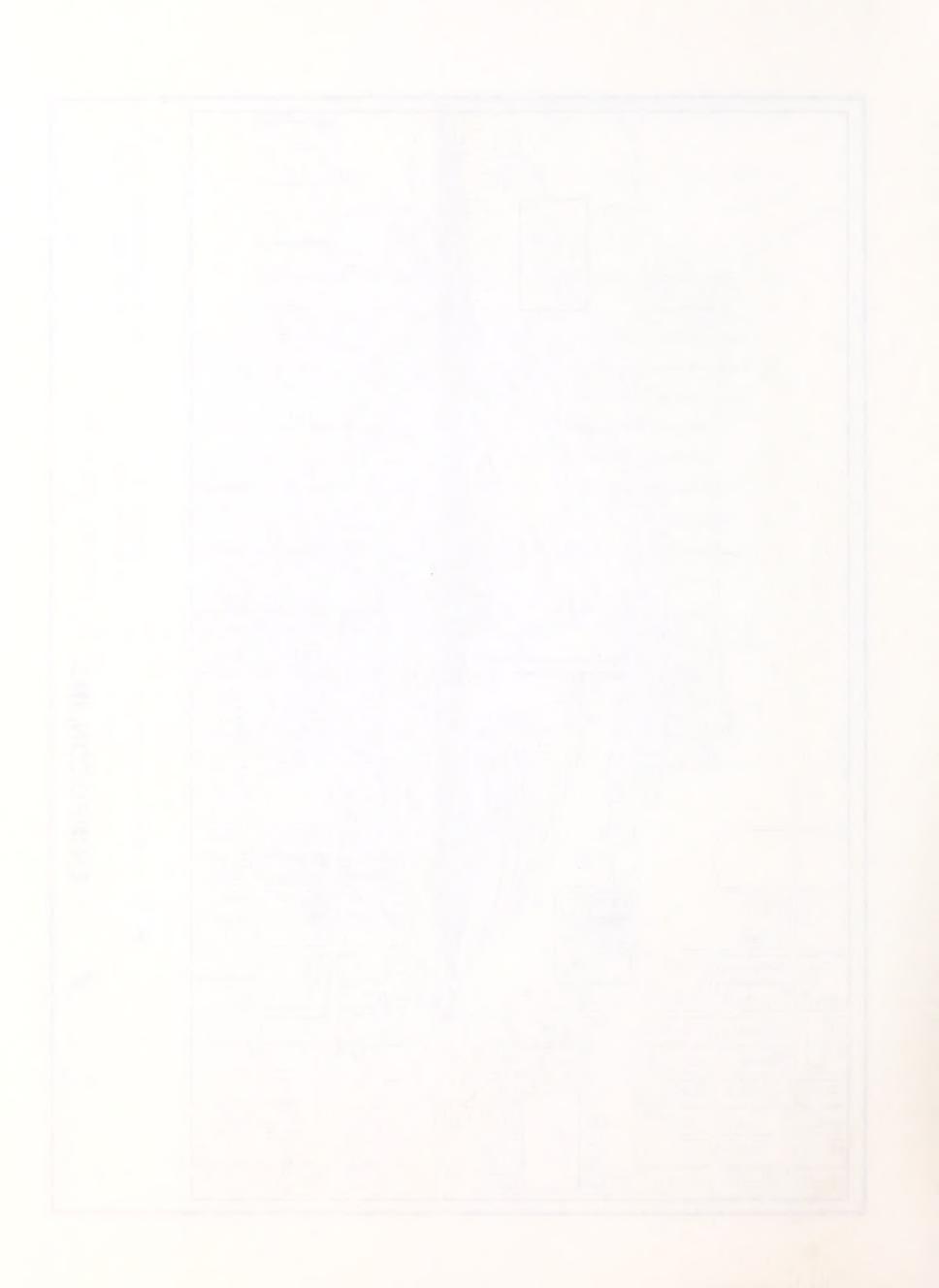
**Table 1.0 - Ambient Air Monitoring Locations** 

Station No.	Universal Time Meridian (UTM)	UTM	East Latitude	North Latitude
1	334050	5056410	45° 38' 36"	113° 7' 46"
2	335360	5057520	45° 39' 13"	113° 6' 47"

 $\overline{\text{UTM ZONE}} = 12$ 

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#### 2.2 Monitoring Parameters

Envirocon designed the ambient air monitoring system to measure PM-10, TSPs, PNAs, and airborne metals. The state of Montana and the Environmental Protection Agency (EPA) have PM-10 and TSP standards. Envirocon's PM-10 and TSP results are compared to these standards to ensure that the standards are not exceeded.

PNA sampling was conducted during the first six sample rounds at Station No. 2. Metal sampling was conducted during the first six sample rounds at both the upwind and downwind stations. Envirocon presented these results in the First Quarterly Ambient Air Monitoring Report. The following is a list of the parameters measured and the methodology used for analysis during the second quarter:

 <u>PM-10</u> - PM-10 is particulate matter less than 10 microns in diameter. Both the upwind and downwind stations have PM-10 samplers.

Method: 40 CFR Part 50, Appendix J.

• <u>TSPs</u> - While PM-10 measurements provide a health-basis comparison for human exposure to particulates, PM-10 does not include all particulates suspended in the atmosphere. A TSP high-volume sampler is used to measure all suspended particulates. The data can be compared to an earlier, out-dated air quality standard for TSPs. That standard was changed in 1987 to a PM-10 methodology.

2.5

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Method: Sections 1.11.1, 2.1.1, and 2.1.1.1 of the Montana Air Quality Assurance Manual

• <u>Meteorology</u> - Envirocon constructed a meteorological tower at Station No. 2 in order to assess what meteorological events may lead to the increase or decrease of ambient air pollutants. The station recorded wind speed, wind direction, temperature, and wind sigma (standard deviation of the wind direction).

Method: Anemometer cup, wind vane, thermocouple, and computer data acquisition system (Ambient Monitoring Guidelines for Prevention of Significant Deterioration [PSD], Section 6, EPA, EPA-450/4-87-007).

### 2.3 Monitoring Frequency

The monitoring frequency for each parameter is shown on Table 2.0.

Table 2.0 - Ambient Monitoring Frequency

PM-10	Once every 6 days, 24-hour duration Station No. 1 and Station No. 2
TSP	Once every 6 days, 24-hour duration Station No. 2 only
Meteorology	Continuous sampling Hourly data analysis Site No. 2 only



#### 3.0 DATA SUMMARY

#### 3.1 PM-10

Envirocon collected 14 PM-10 samples at each station between January 1 and March 31, 1991. The mean PM-10 values for this period were 19 ug/m³ at Station No. 1 and 15 ug/m³ at Station No. 2. The peak PM-10 reporting values for Stations 1 and 2 were 40 ug/m³ and 28 ug/m³, respectively. These values are compared against the Montana ambient air quality standards on Table 3.0.

Table 3.0 - PM-10 Results Versus Ambient Standards

	Standard	Station No. 1	Station No. 2
Mean	50*	19	15
Peak	150**	40	28

Units: ug/m<sup>3</sup>

Complete PM-10 data and summary statistics are provided in Appendix A. The statistics include monthly means, yearly mean to-date, geometric mean and standard deviation. Appendix B contains the results of calibrations, audits and precision checks.

<sup>\*</sup> Annual mean

<sup>\*\*</sup> Not to be exceeded more than once per year



#### 3.2 TSPs

Envirocon operated one TSP sampler at the downwind monitoring station. Envirocon collected 15 TSP samples between January 1 and May 31, 1991. The mean TSP value for this period was 36 ug/m³ and the peak TSP value was 62 ug/m³. These values are compared against the Montana's outdated ambient air quality standards on Table 4.0.

Table 4.0 - TSP Results Versus Outdated Ambient Standards

	Standard	Station No. 2
Mean	75*	36
Peak	260**	62

Units: ug/m<sup>3</sup>

Complete TSP data and summary statistics are in Appendix A. The statistics include monthly means, yearly mean to-date, geometric mean and standard deviation. Appendix B provides quality control information, including calibration and auditing results.

<sup>\*</sup> Annual mean

<sup>\*\*</sup> Not to be exceeded more than once per year



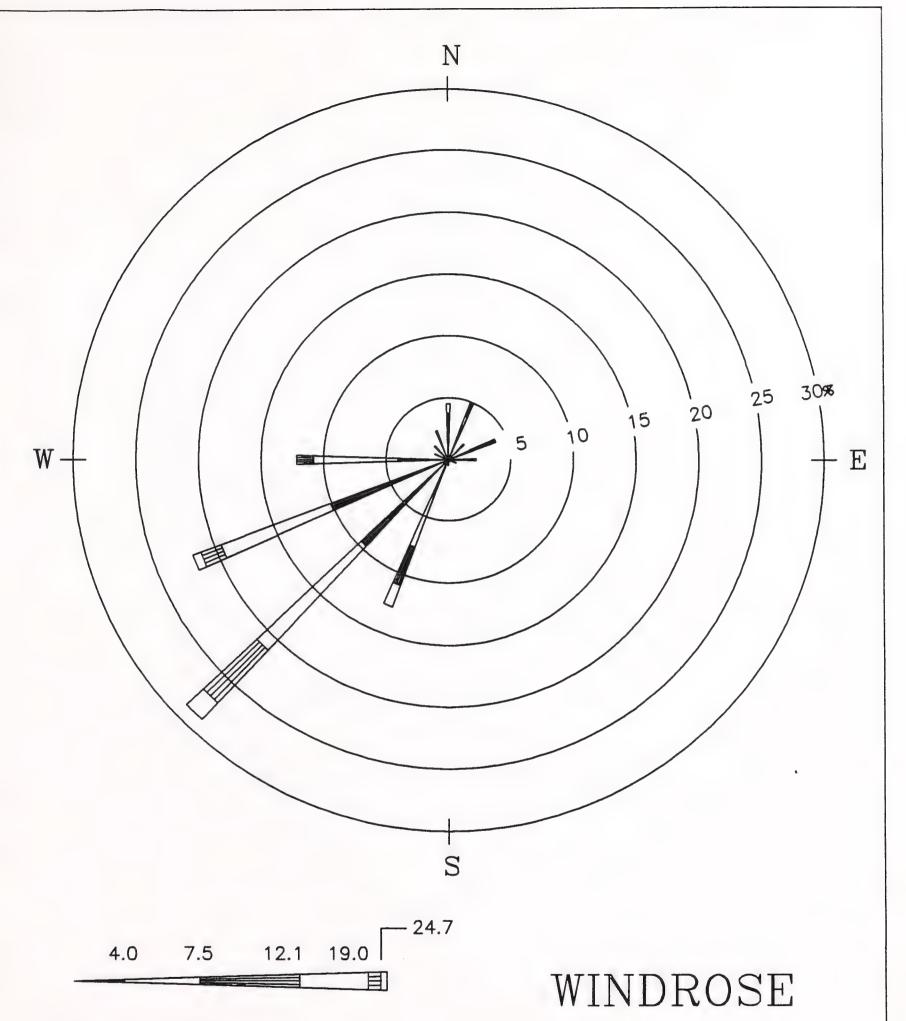
#### 3.3 Meteorology

The meteorological station at the downwind site measures wind speed, wind direction, temperature, and wind sigma. Overall data recovery for the meteorological system was good during the second quarter of operation. Data from 14 days in January and 4 days in March is missing due to a corrupted data file. This data is not recoverable.

Between January 1 and March 31, 1991, the average wind speed was 13.2 miles per hour, the resultant wind direction was 236 degrees, and the percentage of calm hours was 0.0 percent. The maximum temperature during this period was 64 °F, the minimum temperature was -11 °F, and the average temperature was 35 °F.

Appendix A contains a complete list of the meteorological information for wind speed, direction, temperature, and sigma. Appendix A also contains monthly and seasonal wind-frequency distribution data. Windroses are shown on Figures 2.0 through 5.0.





Wind Speed Class Boundaries (Miles/Hour)

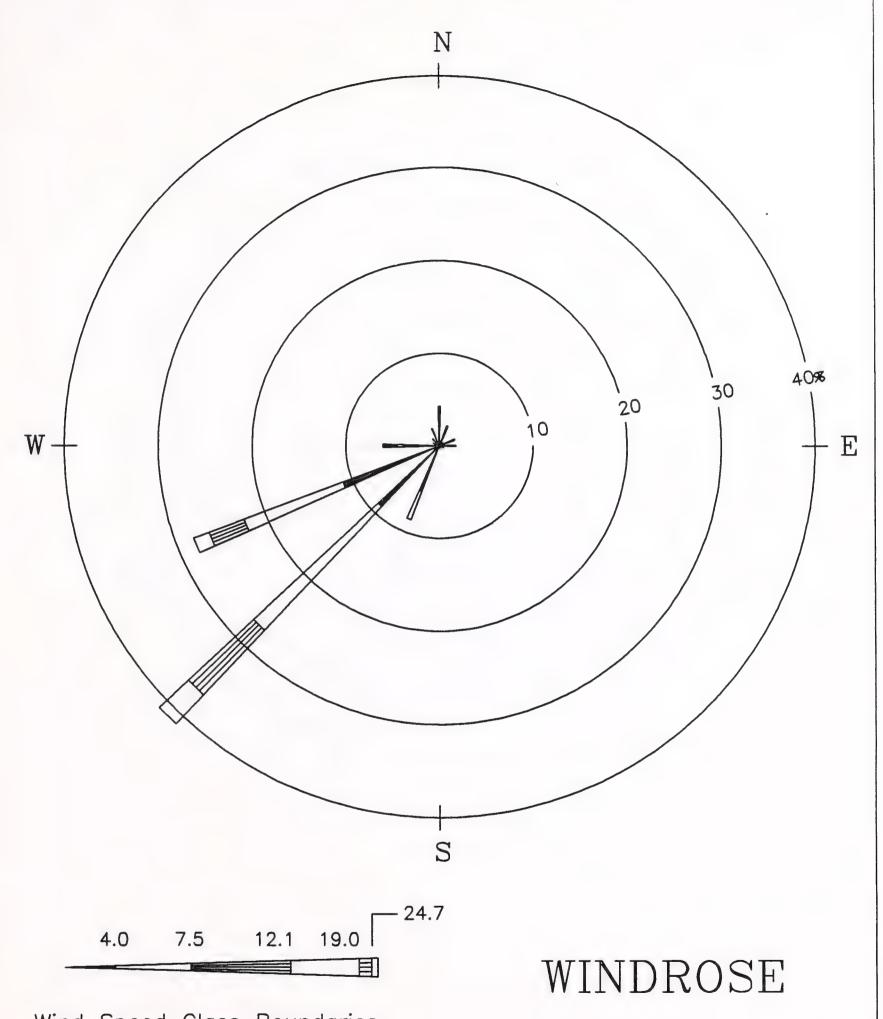
#### NOTES:

Diagram of the Frequency of Occurrence for each Wind Direction. Wind Direction is the Direction From Which the Wind is Blowing. Livingston - Downwind PERIOD: 1 QTR 1991

FIGURE 2.0







Wind Speed Class Boundaries (Miles/Hour)

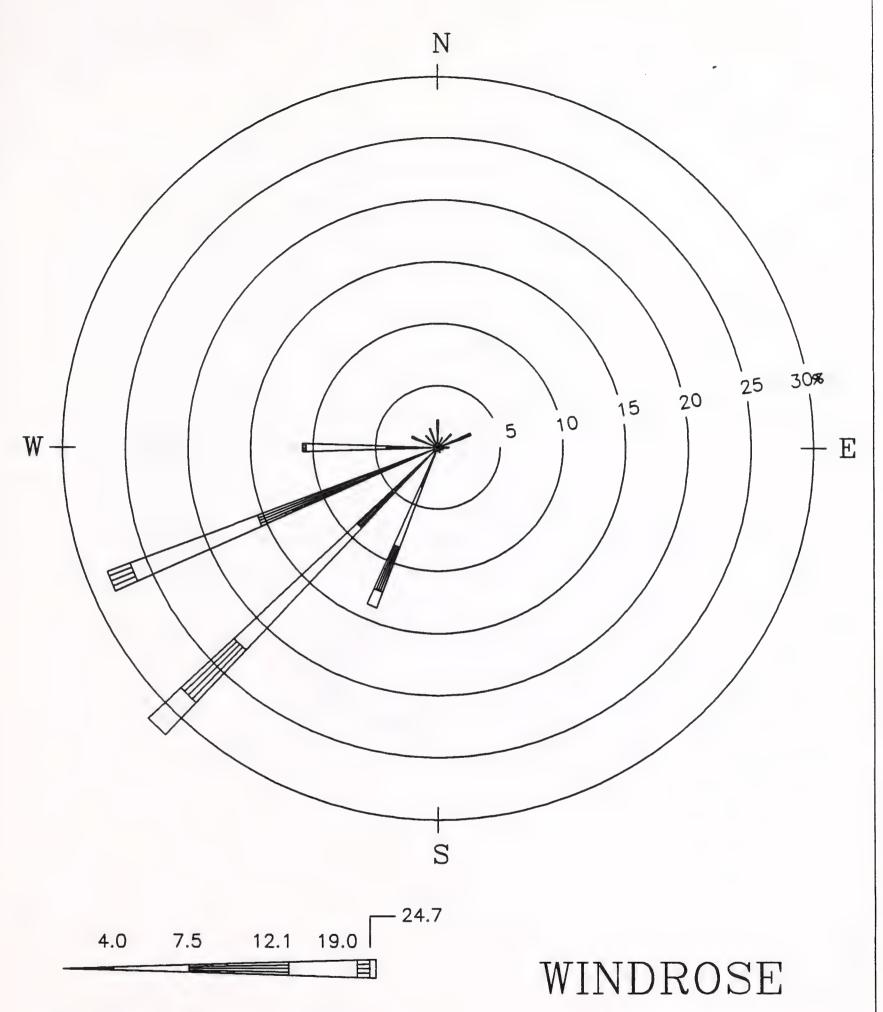
#### NOTES:

Diagram of the Frequency of Occurrence for each Wind Direction. Wind Direction is the Direction From Which the Wind is Blowing. Livingston - Downwind PERIOD: Jan. 1991

FIGURE 3.0

Bison Engineering





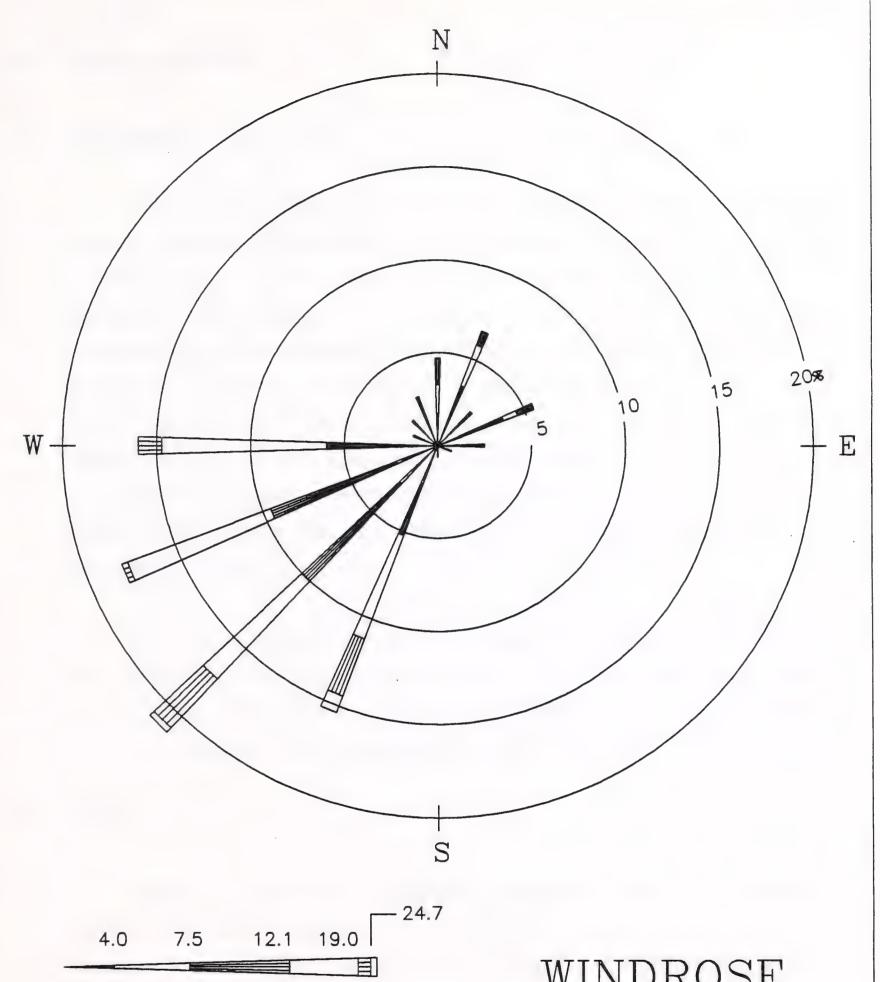
Wind Speed Class Boundaries (Miles/Hour)

#### NOTES:

Diagram of the Frequency of Occurrence for each Wind Direction. Wind Direction is the Direction From Which the Wind is Blowing. Livingston - Downwind PERIOD: Feb. 1991

FIGURE 4.0
Bison





Wind Speed Class Boundaries (Miles/Hour)

#### NOTES:

Diagram of the Frequency of Occurrence for each Wind Direction. Wind Direction is the Direction From Which the Wind is Blowing.

## WINDROSE

Livingston - Downwind PERIOD: Mar. 1991

FIGURE 5.0





#### 4.0 DATA ANALYSIS

#### 4.1 <u>Introduction</u>

The purpose of the ambient air monitoring network is to assess the impacts of existing site contamination and remedial activities on ambient air quality. However, the ambient air monitoring network can not distinguish between sources associated with previous site contamination and sources associated with current industrial operations. The first step of assessment is to measure parameters which could be reasonably expected to enter the ambient atmosphere. These parameters, defined by Section 14.4 of the IRMWP, include PM-10, TSPs, metals, and PNAs. The second step of assessment is to compare these results with previously established ambient air quality standards. The final step of assessment is to compare the results with background results.

This report does not provide the investigative details for each of the above activities; however, it does assess some of the characteristics of the results to date. The following is a discussion of PM-10 and TSP results. Metal and PNA results were discussed in the first quarterly report.

#### 4.2 <u>PM-10</u>

Section 3.0 of this report provided a comparison between the collected PM-10 values and the Montana and EPA ambient air quality standards. The results indicate values well below these standards. All information collected to date indicates that the standards will not be exceeded. Envirocon compared the upwind and downwind PM-10 data and the results of this comparison are provided on Table 7.0.



Table 7.0 - Upwind/Downwind PM-10 Comparison

SAMPLE DATE	UPWIND	DOWNWIND	DIFFERENCE
1/6/91	N/A	17	
1/12/91	14	N/A	
1/18/91	13	13	0
1/24/91	15	9	6
1/30/91	22	24	-2
2/5/91	15	12	3
2/11/91	19	18	1
2/17/91	9	14	-5
2/23/91	15	13	2
3/1/91	19	8	11
3/7/91	12	15	-3
3/14/91	39	28	11
3/19/91	40	20	20
3/25/91	13	8	5
3/31/91	16	15	1

Units: ug/m³

Paired and unpaired t-tests were applied to the data to assess whether there is enough evidence to reject the null hypothesis that the two means are the same. The results of these tests are summarized on Table 8.0.



Table 8.0
Summary Statistics

UPWIND	Mean: Std Dev: No. of Samples:	18.64 9.07 14
DOWNWIND	Mean: Std Dev: No. of Samples:	15.29 5.60 14
DIFFERENCE	Mean: Std Dev: No. of Samples:	3.85 6.58 13

### Comparison of Upwind and Downwind Means

#### Paired Difference t-test:

 $t = Mean/(S/(n)^{5})$  where s = std. dev.

t = 2.11

Critical t (95%) = 2.17

### Unpaired t-test:

 $t = (mean1 - mean2)/(S*(1/n+1/n)^{5})$  where s = pooled std. dev.

t = 1.21

Critical t (95%) = 2.12

Since both t values fall within their respective 95-percent two-tailed confidence intervals (as defined by the critical t values), Envirocon concludes that not enough evidence exists to reject the null hypothesis. Therefore, there



is no difference in the mean and mean-difference PM-10 values between the two monitoring sites.

#### 4.3 <u>TSP</u>

The results of TSP sampling to date indicate values well below the outdated ambient air quality standard. These results are shown in Section 3.0. The IRMWP requires that Envirocon compare three TSP samples where the wind speed exceeded 15 knots (17 mph) during sample collection. The purpose of this comparison is to determine whether TSP values increase during higher wind speeds. Two sample days during the previous quarter exhibited wind speeds exceeding 17 miles per hour and those results were examined in the First Quarterly Ambient Air Monitoring Report. The results of current TSP sampling are compared against the daily mean wind speed for the respective sampling days on Table 9.0.



Table 9.0 - TSP Versus Wind Speed TSP

SAMPLE DATE	(ug/m^3)	(mph)
1/18/91	37	23.1
1/24/91	18	11.2
1/30/91	62	26.5
2/5/91	30	15.8
2/11/91	61	15.3
2/17/91	38	10.9
2/23/91	30	9.4
3/7/91	29	17.2
3/14/91	41	2.4
3/19/91	43	5.3
3/25/91	18	13.5
3/31/91	38	14



Figure 6.0 shows a graph of TSP versus wind speed data. The least-squares regression line is plotted on the figure. The correlation coefficient is 0.29. From a statistical viewpoint, this indicates that about 8% of the data fits the linear model well. This means that there is little or no relation between wind speed and TSP concentrations.



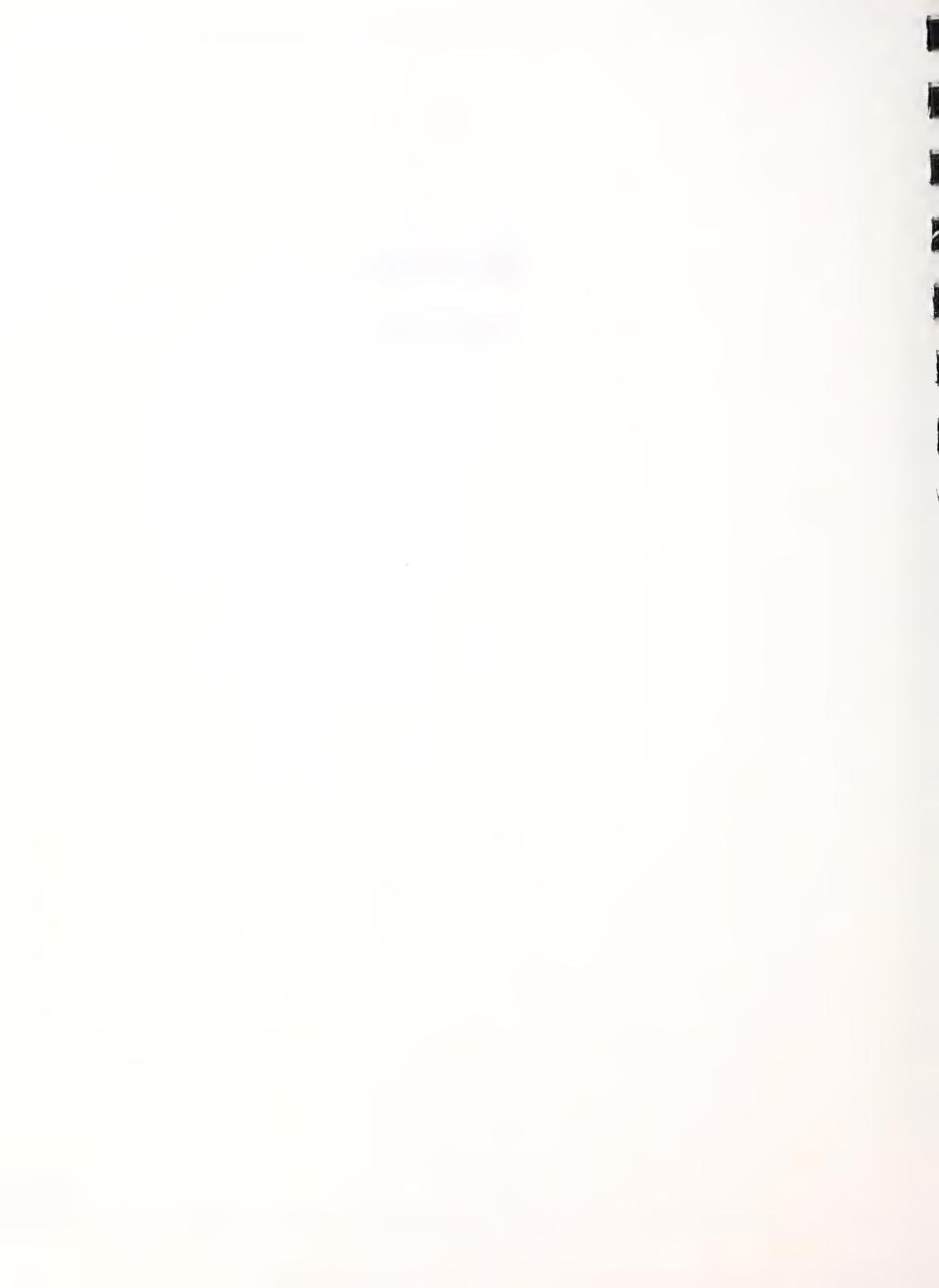
### APPENDIX A DATA RESULTS

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### PM10 Data

(Appendix A)





### Bison Engineering Inc

Helena, MT 59601

### PM10 Particulate Summary

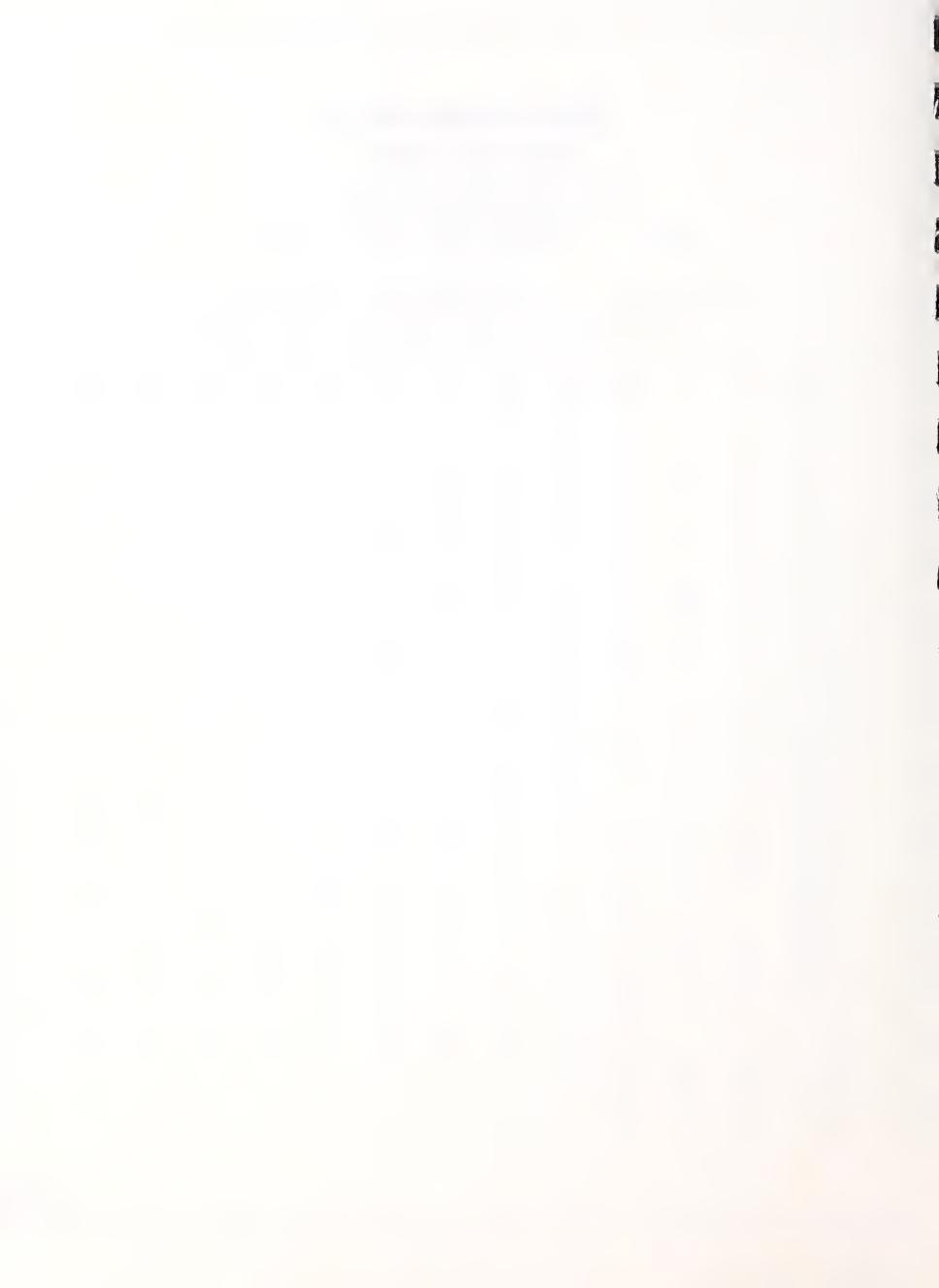
1991 Site & Area: 1111 3

Upwind Site Livingston, MT Envirocon

(Values are in Micrograms per Cubic Meter)

Day	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	oct	Nov	Dec
1	-	_	19	-	_	_	_	-	-	_	-	_
2	-	_	_	953	_	-	_	_	-	-	-	-
3	-	-	_	_	-	_	-	***	-	_	-	-
1 2 3 4 5 6 7 8 9	-	-	-	-	-	-	_	_	-	400		-
5		15	_	_	_	-	_	-	_	-	_	-
6	***	-	-	_	_	-	-	-	-	_	_	-
7	-	-	12	-	_	_	-	-	-	_	_	_
8	-	-	-	-	-	-	-	-	_	-	***	_
9	-	-	-	-	_	_	_	-	-	-	-	_
10	-	-	-	_	-	***	***	-	***************************************	-	_	
11	-	19	-	_	-	_	-	-	-	-	-	-
12	14	****	_	_	-	-	_	-	***	_	_	_
13	_	_	_	_	_	_	_	_	_	_	_	-
14 15	-	_	39	_	_	_	_	_	_	_	<del>-</del>	-
15	_	_	_	_	_		-	_	-	-	_	-
16	-	-	_	_	_	-	_	-	_	-	_	-
17	-	9	-	-	-	-	_	-	_	_	_	-
18	13	_	_	_	_	-	-	-	-	-	_	-
19	-	_	40	-	•••	-	_	-	_	-	_	_
20	_	_	-	-	_	-	-	_	_	_	-	_
21	_	-	_	_	-	-	-	-	-	-	-	-
22	-	-	-	-	-	_	_	_	_	_	-	-
23	-	15	-	-	-	-			-	-	_	-
24	15	_	-	-	-	-	_	-	-	-	_	-
25	_	-	13	-	-	-	_	-	_	-	_	-
26	-	_	-	-	-	_	-	-	_	_	_	-
27	_	_	-	-	-	-	-	-	-	-	_	-
28	_	-	-	-	***	-	-	*	-	-	-	-
29		_	-	-	_	-	_	-	_	-	-	-
30	22	_	-	-	-	-	-	-	_	_	_	
31		-	16	-	-	-	-	-	-	-	-	-
No.	4	4	6	0	0	0	0	0	0	0	0	0
Max	22	19	40									
Avg	16	15	23									





### Bison Engineering Inc

Helena, MT 59601

### PM10 Particulate Summary

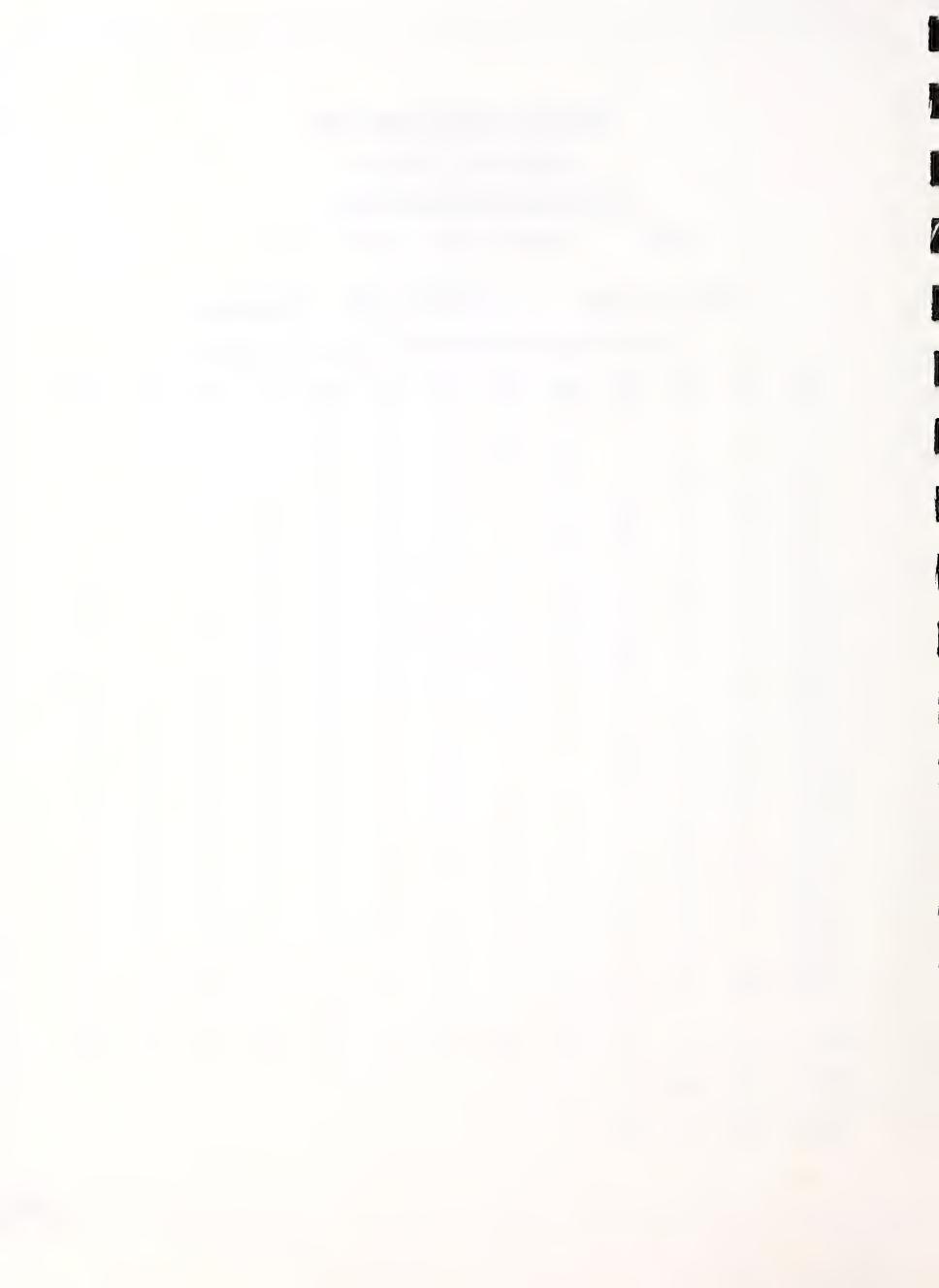
1991 Site & Area: 1111 4

Downwind Site Livingston, MT Envirocon

(Values are in Micrograms per Cubic Meter)

Day	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	-	-	8	-	-	-	-	-	-	_	-	-
2	-	-	-	-	-	-	-	-	_	_	_	-
3	-	-	-	-	-	-	-	_	-		-	-
4	-	-	-	_	_	-	-		-	_	-	-
1 2 3 4 5 6 7	-	12	-	-	-	-	-	-	-	_		_
6	17	-	-	-	-	_	_	-	_	-	-	-
	-	_	15	-	-	-	-	-	_	_	-	-
8 9		_	-	-	-	_	_	-	_	•••	-	-
9	-	_	-	-	-	_	_	_	_	_	****	-
10	-	-	-	-	-	-	_	-	_	_	-	-
11	-	18	-	-	-	-	-	-	***	_	-	-
12	-	-	-	•	-	***	-	-	-	_	-	_
13	_	-	-	-	-	_	-	-	_	-	-	-
14 15	-	-	28	-	-	_	_	-	-	-	-	-
15	-	-	-		-	-	-	-	-	_	-	-
16	-	-	-	-	-	•	-	-	-	_	_	-
17	-	14	***	-	_	_	_	-	-	_	-	_
18	13	_	_	-	-	_	-	_	_	_	*****	-
19	_	_	20	-	-	-	_	-	-	-	_	-
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21	-	_	-	-	-	-	_	-	-		_	-
22	_	_	-	-	-	-	_	_	-	_	_	-
23	-	13	_	_	_	-	_	-	_	_	_	-
24	9	-	-	-	***	_	_	_	_	_	_	-
25	_	_	8	_	-	_	_	_	_	_	-	-
26	-	-	-	-	-	-	_	_	_	_	_	-
27	-	-	-	-	-	***	-	_	-	-	-	-
28	***	-	-	_	_	-	***	-	-	-	electric	-
29	-	_	-	-	_	-	_	_	_	_	-	-
30	24	_	-	-	-	_	_	_	_	_	-	-
31	-	-	15	-	-	-	-	-	-	-	-	-
No.	4	4	6	0	0	0	0	0	0	0	0	0
Max	24	18	28									
Avg	16	14	16									





### Bison Engineering Inc. Helena, MT 59601

# SUMMARY STATISTICS FOR THE PM10 PARTICULATE DATA

1991

	Total # Obs.	14	14
on	Geo. Std Dev	1.5	1.5
Envirocon	Geo. Mean	17	14
Livingston, MT	Arith. Std Dev	Q	9
Livingst	Arith. Mean	19	15
	150	0	0
	2nd Max	39	24
Upwind Site	Max	40	28
Upwi	Min	6	ω
	Site #	8	4





### **TSP** Data

(Appendix A)



			1
			14

### Bison Engineering Inc

Helena, MT 59601

### Total Suspended Particulate Summary

1991

Site & Area: 1111

4

Downwind Site Livingston, MT Envirocon (Values are in Micrograms per Cubic Meter)

Day	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1 2 3	_	_	20	-	_	_	-	-	_	-	_	-
2	-	_	_	_	_	-	_	-	-	_	_	_
	code	_	_	-	-	_	_	_	_	_	-	_
4	-	_	-	_	_	_	_	_	_	-	-	-
5	-	30	_	_	_	_	_	-	-		-	-
4 5 6 7	33	_	_	_	_	-	-	-	_	_	-	-
7	_	_	29	-	-	-	_	-	4000	4000	_	-
8	_	_	-	-	_	-	_	-	_	_	-	_
9	-	_		_	-	-	-	-	_	_	_	-
10	_	-	-	-		_	-	_	_	_	_	-
11	_	61	-	-	-		-	-	_	_	-	-
12	43	-	-	-	-	-	-	-	-	-	-	-
13	-		-	-	-	-	_	-	_	-	-	-
14	-		41	-	-	-	-	_	_	-	_	-
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23	_	30	_	_	-	-	-	-	-	_	-	_
24	18	-	_	-	-	_	-	-	_	_	_	-
25	-	_	18	-	-	-	_	_	_	_	_	-
26	-	_	_	-	_	-	_	_	-	-	_	-
27	-	_	_	-	-	_	-	-	-	_	_	-
28	_	_	_	_	-	-	_	-	_	-	_	_
29	-	_	-	_	-	-		_	_	-	_	-
30	62	_	_	-	_	-	_	-	_	-	-	-
31	-	-	38	-	-	-	-	-	-	-	-	-
No.	5	4	6	0	0	0	0	0	0	0	0	0
Max	62	61	43									
Avg	39	40	32									





### Bison Engineering Inc. Helena, MT 59601

# SUMMARY STATISTICS FOR THE TSP PARTICULATE DATA

*	•	-	
_			
C	J	)	
C	7	1	
		9	
8			

	Total # obs.	15
con	Geo. Std Dev	1.5
Envirocon	Geo. Mean	34
Livingston, MT	Arith. Std Dev	13
Living	Arith. Mean	36
	# >	0
Site	2nd Max	61
Downwind Site	Max	62
Dow	Min	18

Site #





Meteorological Data (Appendix A)

## JANUARY 1991

## \*\*\* WIND SPEED SUMMARY \*\*\*

AVG.			a		•		•		•	•			•	•	•	9.01	12.1	15.5	23.1	12.3	12.5	18.4	12.6	11.3	11.2	7.9	15.8	17.5	14.0		26.5	23.6		
	57	•	•	•		•	•		•		•		•		•	8.0	11.0	19.0	22.0	15.0	14.0	20.0	0.6	18.0	3.0	10.0	14.0	13.0	12.0	24.0	24.0	16.0	14.8	
	23	١	٠	•	١	•	٠	1	•	•	•	ŧ	ı	•	•	9.0	12.0	17.0	29.0	13.0	12.0	21.0	5.0	21.0	5.0	8.0	19.0	18.0	10.0	22.0	24.0	21.0	15.6	
	22	٠	•	•	•	•	•		•	•	•	•	٠	•		7.0	13.0	19.0	29.0	12.0	13.0	21.0	5.0	21.0	3.0	7.0	16.0	23.0	2.0	23.0	29.0	19.0	15.4	
	21	•	•		•	•	٠	•	1	1		•	•	•	•	5.0	12.0	16.0	27.0	0.6	11.0	21.0	7.0	20.02	8.0	8.0	15.0		2.0	20.0	29.0	21.0	14.9	
	20	•	•	•	•	•	١	٠	•	•	•	•	•	•	•	8.0	13.0	17.0	22.0	7.0	10.0	20.02	10.0	17.0	10.0	10.0	15.0	17.0	0.9	24.0	28.0	21.0	15.0	
	19	•	•		•	•	•	٠		•	•	•	•	•	•	11.0	12.0	19.0	20.02	0.6	8.0	22.0	12.0	15.0	15.0	8.0	16.0	12.0	13.0	25.0	24.0	21.0	15.4	
	18	٠	٠	•	•	٠		•	•	•	•	•	•	•	•	12.0	13.0	15.0	19.0	9.0	10.0	23.0	0.6	13.0	16.0	11.0	16.0	18.0	11.0	32.0	29.0	22.0	16.4	
	17	•	٠		1	•	•	•	•	•	•	•	•	•		13.0	14.0	14.0	23.0	12.0	13.0	20.0	10.0	10.0	12.0	8.0	15.0	17.0	13.0	26.0	33.0	22.0	16.2	
	16	•	4	•		•	1	1	•	•	•	•	•	•	•	11.0	17.0	17.0	20.0	16.0	15.0	21.0	12.0	11.0	13.0	7.0	18.0	20.0	12.0	27.0	34.0	25.0	17.4	
	15	•	•	•	•	•	•	•	•	•	•	•	•	•	•	14.0	17.0	14.0	26.0	16.0	14.0	20.02	14.0	11.0	12.0	0.9	23.0	20.0	17.0	25.0	32.0	24.0	17.9	
	14	1	ι	•	٠	•	•	•	•	٠	•	•	t	•		16.0	17.0	14.0	25.0	18.0	13.0	19.0	14.0	11.0	14.0	0.6	16.0	18.0	16.0	21.0	27.0	24.0	17.2	
ß	13	•	•	•	•	•	•	•	•	•	•	•		•	•	13.0	20.0	11.0	24.0	16.0	13.0	20.0	13.0	11.0	0.6	10.0	12.0	23.0	16.0	22.0	26.0	21.0	16.5	53.6
HOURS	12	•	٠	ı	•	٠	•	•	•	•	•	•	•	٠	•	12.0	14.0	12.0	22.0	14.0	13.0	19.0	11.0	13.0	0.6	11.0	15.0	14.0	20.0	23.0	23.0	20.0	15.6	II S
H	1	•	•	•	•	•	•	•	r	•	•	•	•	•	•	11.0	14.0	14.0	24.0	9.0	13.0	19.0	13.0	6.0	11.0	15.0	16.0	17.0	20.0	23.0	23.0	23.0	15.9	tenes
	10	•	٠	٠	•	•	•	•	٠	•	•	•	•	•	•	0.6	13.0	13.0	27.0	10.0	11.0	20.0	13.0	3.0	9.0	14.0	18.0	22.0	23.0	24.0	28.0	21.0	16.4	Comple
	6	•	•	•	•	•	ı	•	•	•	•	•		•	•	•	11.0	14.0	24.0	7.0	10.0	16.0	15.0	2.0	0.9	12.0	14.0	21.0	23.0	25.0	28.0	25.0	15.8	Data C
	8	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	9.0	16.0	18.0	4.0	11.0	16.0	15.0	0.9	8.0	12.0	15.0	18.0	21.0	27.0	27.0	27.0	15.6	× 0
	7		•	•	1	•	•	•	•	•	•	•	•	t	•	١	9.0	15.0	21.0	0.6	12.0	17.0	18.0	5.0	10.0	4.0	16.0	21.0	17.0	24.0	25.0	27.0	15.6	
	9	•	•	•		•	•		•	1	•	•	•	•	•	•	10.0	18.0	25.0	10.0	13.0	17.0	20.0	5.0	11.0	4.0	17.0	17.0	17.0	23.0	25.0	29.0	16.3	2
	2		•	•	•	•	•	•	•	ı	•	•	1	•	•	1	8.0	18.0	21.0	16.0	16.0	15.0	17.0	11.0	14.0	3.0	17.0	10.0	15.0	24.0	25.0	30.0	16.3	399
	4	١	•	•	٠	ı	1	•	•	•	•	•	•	•	٠	•	9.0	17.0	20.0	18.0	14.0	13.0	14.0	13.0	17.0	3.0	14.0	14.0	14.0	19.0	25.0	28.0	15.8	Hours =
	м	٠	•	•	•	1	٠	•	•	•	1	•	•	•	٠	•	9.0	15.0	23.0	11.0	13.0	14.0	14.0	4.0	19.0	3.0	14.0	16.0	15.0	19.0	22.0	27.0	14.9	jq
	2	•	•	•	1	•	•	•	•	•	•	•	•	•	•	٠	9.0	15.0	23.0	16.0	14.0	15.0	16.0	9.0	18.0	3.0	15.0	13.0	16.0	15.0	21.0	26.0	15.3	of Val
	-	•	•	•	ı	•	•	1	•	•	•		٠	•		٠	4.0	13.0	21.0	18.0	14.0	13.0	16.0	15.0	17.0	3.0	14.0	15.0	5.0	13.0	26.0	27.0	14.6	*
DAY		-	2	ĸ	4	50	9	7	∞	0	10	=	12	13	14	15	16	17	18	19	20	21	22	23	5%	52	56	27	28	53	30	31	AVG.	





## FEBRUARY 1991

## \*\*\* WIND SPEED SUMMARY \*\*\*

### HOURS

AVG. 15.5 8.0 11.8 13.5 16.3 10.9 15.8 5.3 17.2 11.5 15.3 16.7 9.3 8.7 11.7 20.5 9.1 21.5 12.1 4.6 13.0 15.0 15.0 14.0 23.0 24.0 19.0 26.0 25.0 25.0 22.0 21.0 23.0 25.0 21.0 18.0 16.0 14.0 12.0 23.0 21.0 24.0 25.0 25.0 6.0 7.0 11.0 12.0 13.0 15.0 15.0 21.0 21.0 16.0 14.0 14.0 14.0 14.0 14.0 11.0 8.0 11.0 8.0 10.0 8.0 7.0 7.0 9.0 21.0 21.0 22.0 21.0 22.0 25.0 25.0 25.0 27.0 28.0 26.0 26.0 26.0 24.0 22.0 20.0 20.0 21.0 19.0 21.0 18.0 18.0 18.0 18.0 19.0 19.0 18.0 16.0 15.0 16.0 18.0 16.0 17.0 16.0 16.0 15.0 17.0 18.0 14.0 13.0 9.0 8.0 13.0 13.0 18.0 15.0 17.0 16.0 17.0 20.0 17.0 17.0 15.0 16.0 15.0 15.0 15.0 16.0 21.0 25.0 27.0 25.0 22.0 21.0 24.0 25.0 28.0 28.0 24.0 24.0 29.0 27.0 5.0 6.0 4.0 3.0 2.0 2.0 2.0 2.0 1.0 2.0 13.0 12.0 6.0 6.0 6.0 7.0 6.0 5.0 7.0 7.0 4.0 4.0 6.0 10.0 13.0 17.0 17.0 17.0 15.0 19.0 23.0 23.0 23.0 26.0 20.0 22.0 19.0 17.0 14.0 16.0 15.0 15.0 12.0 11.0 14.0 15.0 15.0 15.0 16.0 14.0 15.0 14.0 15.0 13.0 15.0 14.0 17.0 16.0 14.0 15.0 15.0 14.0 11.0 12.0 6.0 3.0 6.0 4.0 6.0 4.0 7.0 11.0 9.0 11.0 12.0 11.0 11.0 10.0 14.0 11.0 13.0 14.0 7.0 8.0 6.0 4.0 4.0 6.0 2.0 6.0 9.0 4.0 4.0 3.0 3.0 9.0 14.0 13.0 12.0 11.0 16.0 20.0 22.0 22.0 17.0 20.0 22.0 18.0 15.0 15.0 13.0 11.0 12.0 12.0 15.0 15.0 16.0 17.0 19.0 17.0 13.0 20.0 18.0 16.0 13.0 14.0 18.0 17.0 24.0 20.0 17.0 22.0 18.0 21.0 15.0 9.0 15.0 15.0 13.0 13.0 16.0 12.0 15.0 17.0 13.0 14.0 13.0 15.0 13.0 15.0 16.0 17.0 13.0 14.0 12.0 17.0 17.0 17.0 12.0 10.0 10.0 10.0 10.0 11.0 10.0 10.0 13.0 13.0 10.0 8.0 11.0 14.0 14.0 9.0 7.0 9.0 13.0 11.0 7.0 5.0 6.0 5.0 8.0 6.0 5.0 10.0 9.0 9.0 10.0 12.0 14.0 13.0 12.0 13.0 14.0 17.0 17.0 18.0 23.0 21.0 18.0 16.0 11.0 16.0 17.0 14.0 18.0 18.0 20.0 17.0 17.0 17.0 17.0 17.0 14.0 12.0 8.0 8.0 9.0 9.0 11.0 12.0 9.0 10.0 9.0 9.0 6.0 5.0 5.0 8.0 12.0 11.0 8.0 7.0 6.0 4.0 8.0 11.0 12.0 9.0 7.0 9.0 10.0 11.0 13.0 14.0 12.0 11.0 13.0 13.0 15.0 14.0 15.0 10.0 8.0 8.0 5.0 7.0 10.0 11.0 10.0 14.0 13.0 9.0 9.0 6.0 11.0 12.0 12.0 12.0 13.0 17.0 15.0 18.0 18.0 15.0 12.0 10.0 9.0 10.0 9.0 9.0 8.0 9.0 11.0 14.0 16.0 19.0 21.0 22.0 20.0 21.0 16.0 20.0 20.0 23.0 33.0 30.0 26.0 26.0 25.0 23.0 24.0 22.0 24.0 21.0 18.0 21.0 21.0 19.0 20.0 22.0 24.0 25.0 27.0 30.0 27.0 20.0 21.0 21.0 23.0 24.0 17.0 18.0 20.0 20.0 22.0 17.0 13.0 12.0 16.0 12.0 7.0 8.0 7.0 5.0 1.0 1.0 1.0 1.0 9.0 14.0 13.0 12.0 14.0 16.0 16.0 14.0 13.0 6.0 6.0 20.0 16.0 6.0 6.0 5.0 4.0 2.0 2.0 2.0 2.0 1.0 1.0 6.0 16.0 19.0 17.0 17.0 17.0 11.0 8.0 7.0 10.0 14.0 11.0 19.0 10.0 6.0 9.0 10.0 10.0 8.0 8.0 6.0 9.0 4.0 4.0 4.0 7.0 14.0 16.0 11.0 15.0 13.0 10.0 8.0 6.0 6.0 11.0 11.0 17.0 18.0 15.0 17.0 17.0 16.0 18.0 17.0 12.0 13.0 11.0 18.0 19.0 23.0 16.0 20.0 22.0 23.0 20.0 21.0 20.0 20.0 17.0 18.0 18.0 18.0 25.0 27.0 27.0 24.0 23.0 21.0 20.0 16.0 15.0 16.0 14.0 15.0 12.0 11.0 14.0 17.0 17.0 14.0 10.0 10.0 12.0 9.0 5.0 4.0 10.0 11.0 13.0 14.0 15.0 9.0 12.0 8.0 18.0 18.0 20.0 16.0 17.0 16.0 17.0 16.0 11.0 9.0 3.0 5.0 11.0 9.0 7.0 5.0 9.0 6.0 12.5 13.0 13.0 12.5 12.9 13.3 14.0 14.3 14.3 15.0 15.7 16.2 16.5 15.5 15.0 15.0 13.9 12.2 11.3 11.8 12.6 12.0 12.1 12.3 23 6.0 5.0 3.0 3.0 3.0 3.0 6.0 4.0 5.0 9.0 10.0 12.0 14.0 17.0 17.0 18.0 13.0 11.0 11.0 11.0 11.0 2.0 8.0 13.0 12.0 13.0 14.0 13.0 11.0 8.0 13.0 11.0 12.0 10.0 9.0 7.0 4.0 6.0 5.0 7.0 9.0 12.0 14.0 9.0 10.0 12.0 13.0 16.0 16.0 22.0 21.0 15.0 13.0 10.0 11.0 15.0 14.0 13.0 8.0 4.0 7.0 7.0 8.0 20 19 18 17 16 15 14 13 % Data Completeness = 100.0 12 7 10 8 9 of Valid Hours = 672 5.0 11.0 12.0 6.0 9.0 5.0 13 16 8 19 11 12 14 15 17 DAY





### **MARCH 1991**

## \*\*\* WIND SPEED SUMMARY \*\*\*

HOURS

				и	•	1	0				2	M	2	<u>u</u>	7		9					%	AVG
1 2 3 4 5 6 7 8	4	4 5 6 7 8	2 9 5	8 / 9	8	×		0	0	=	12	13	4	2	9	_	2	<b>S</b>	50 21	77	S	47	
			•	•	•							•						•			•	1	•
		1 1	•	1					1			•	,		•							•	•
•	1	•	•	•	,	1											•	,		,	•	•	1
			•	•	•							•										•	•
				•	•				- 10	0.	0.	0.9	7.0 16	0.	18.0 14	4.0 12	2.0 11	0.	0.0	.0 14.0	14	0 12.0	11.8
10.0 10.0 10.0 8.0 8.0 13.0 17.0 14.0 1	.0 8.0 8.0 13.0 17.0 14.0	8.0 13.0 17.0 14.0	.0 13.0 17.0 14.0	.0 17.0 14.0	14.0	0.	CO.	18.0 16	5.0 15	0.	0.	17.0 17	0	0	16.0 15	0.	10.01	1.0 14	.0 11	0.6 0.		0 12.0	12.9
12.0 11.0 13.0 14.0 15.0 12.0 14.0 16.0 19	.0 14.0 15.0 12.0 14.0 16.0	15.0 12.0 14.0 16.0	.0 12.0 14.0 16.0	14.0 16.0	16.0			19.0 20	0.0	1.0 19	0.	21.0 23	3.0 19	0.	19.0 23	3.0 23	3.0 20	0.	0.	20.0 14.0	.0 10.0	0 11.0	17.2
14.0 13.0 12.0 8.0 6.0 5.0 7.0 11.0 1	8.0 6.0 5.0 7.0 11.0	6.0 5.0 7.0 11.0	5.0 7.0 11.0	7.0 11.0	11.0	0.	N	12.0 14	.0 1	5.0 17	0.	19.0 20	0.0 19	0.	18.0 16	5.0 12	2.0 11	.0 15	.0 19	.0 23.0	20	0 21.0	14.5
24.0 23.0	22.0 25.0 24.0 24.0 23.0	25.0 24.0 24.0 23.0	24.0 24.0 23.0	24.0 23.0	23.0	0.	CA	29.0 27	7.0 22	0.	0.	23.0 24	4.0 23	0.	4.0 20	0.0 23	3.0 22	0	.0 21	.0 18.0	.0 20.0	0.91 0	22.5
15.0 17.0 16.0 15.0 18.0 16.0 19.0 20.0 2	15.0 18.0 16.0 19.0 20.0	18.0 16.0 19.0 20.0	16.0 19.0 20.0	19.0 20.0	20.0		C	22.0 26.	5.0 26	5.0 23	0.	24.0 26	.0 2	0.	0	0.0 21	0.	0	11 0.9	6 0.	9		
2.0 1.0 2.0 8.0 10.0 5.0 10.0	.0 2.0 8.0 10.0 5.0 10.0	8.0 10.0 5.0 10.0	10.0 5.0 10.0	5.0 10.0	.0 10.0		CA	9.0 10	0.0	0.	0.	0.4	0.9	2.0 4	4.0 4	9 0.4	5.0 7	0					
10.0 17.0	.0 12.0 10.0 9.0 10.0 17.0	10.0 9.0 10.0 17.0	9.0 10.0 17.0	10.0 17.0	17.0	0.	0	20.0 20		0.	0	-	.0 1	.01		0	0.	0.		-	-		
.0 12.0 11.0 8.0 6.0 10.0	.0 12.0 11.0 8.0 6.0 10.0	11.0 8.0 6.0 10.0	.0 8.0 6.0 10.0	6.0 10.0	10.0	0.	0	0.0	2 0.	5.0 13	0	12.0	8.0	0.	6.0 5	5.0.5	9 0.9	0.			14	141	
4.0 3.0 2.0 1.0 2.0 1.0 1.0	.0 2.0 1.0 2.0 1.0 1.0	1.0 2.0 1.0 1.0	2.0 1.0 1.0	1.0 1.0	1.0		-	1.0 1		0.	0		0.	0.		0.	0.	0			4		
5.0 4.0 4.0 11.0 10.0 11.0 8.0	4.0 11.0 10.0 11.0 8.0	11.0 10.0 11.0 8.0	10.0 11.0 8.0	11.0 8.0	8.0	0.	-	7.0.7		0.	0		0.	0.	7 0.6	0.		0.			la1	141	
	.0 3.0 3.0 3.0 1.0 2.0	3.0 3.0 1.0 2.0	.0 3.0 1.0 2.0	1.0 2.0	5.0		1.7	2.0 1	1.0 3	0.	0.	0	0.	3.0		0.	6.0 5	0.	4.0 5	5.0 2.0	0.4 0.		3.7
7.0 8.0 8.0 6.0 4.0 3.0 2.0	.0 8.0 6.0 4.0 3.0 2.0	6.0 4.0 3.0 2.0	.0 4.0 3.0 2.0	3.0 2.0	2.0			.0 5		0	0.	8.0	0.	0.	14.0 17	0	0	0.		4	5		
11.0 12.0 14.0 12.0 13.0 14.0 15.0 18.0 21	.0 12.0 13.0 14.0 15.0 18.0	13.0 14.0 15.0 18.0	.0 14.0 15.0 18.0	.0 15.0 18.0	.0 18.0			21.0 16	5.0 13	.01		0	15.0 1	0.		14.0 13		0.			LA .		
3.0 4.0 4.0 4.0 5.0 6.0 4.0	.0 4.0 4.0 5.0 6.0 4.0	4.0 5.0 6.0 4.0	.0 5.0 6.0 4.0	0.4 0.9	0.4			9 0.4		0.		0.	0.	0.		0	0.	0.			w	00	5.3
5.0 5.0 11.0 13.0 11.0 13.0 17.0 19.0 14	.0 13.0 11.0 13.0 17.0 19.0	11.0 13.0 17.0 19.0	.0 13.0 17.0 19.0	17.0 19.0	19.0			14.0 15	.0 15	0.		18.0 17	0.	0.	-	7.0 18	0	0.					13.7
10.0 13.0 11.0 10.0 9.0 11.0 10.0 9.0 1	.0 10.0 9.0 11.0 10.0 9.0	9.0 11.0 10.0 9.0	.0 11.0 10.0 9.0	.0 10.0 9.0	9.0	0.	-	11.0.11	01 0.1	0.	8.0	7.0	0.9	0.	3.0 6	5.0 11	1.0 12	0.		8.0 6.0	7	0 10.0	0.6
12.0 14.0 11.0 11.0 13.0 12.0 14.0 15.0 18	11.0 13.0 12.0 14.0 15.0 1	13.0 12.0 14.0 15.0 1	.0 12.0 14.0 15.0 1	.0 14.0 15.0 1	15.0 1	0.	CE	.0 19	0.0	0.		15.0 17	.01	0.	0.	.01	0			0	12		13.8
11.0 8.0 8.0 8.0 8.0 7.0 7.0	.0 8.0 8.0 8.0 7.0 7.0	8.0 8.0 7.0 7.0	8.0 7.0 7.0	0.7 0.7 0.	7.0	0.	1.0	5.0 4		2.0		0-4	5.0	6.0 13	3.0 10	0.0	0.	2.0	.0 11	.0 12.0	-	16	
14.0 13.0 10.0 9.0 8.0 6.0 6.0 6.0	0.9 0.9 0.9 0.8 0.6 0.	8.0 6.0 6.0 6.0	6.0 6.0 6.0	0.9 0.9	0.9		5	.0 10		0.	0.	12.0 13	3.0 14	0.	18.0 24	4.0 25	0	0.	_	0.	•	0	
5.0 8.0	.0 5.0 3.0 4.0 5.0 8.0	3.0 4.0 5.0 8.0	0.8 0.5 0.4 0.	5.0 8.0	8.0		4	.0 7	-	2.0 1	5.0 2	21.0 23	3.0 21	0.	20.0 14	4.0 20	0.	.0 2	0	24.0 24.0	17	17	
16.0 12.0 12.0 12.0 5.0 10.0 10.0 9.0	.0 12.0 5.0 10.0 10.0 9.0	5.0 10.0 10.0 9.0	.0 10.0 10.0 9.0	.0 10.0 9.0	0.6	0.	9	.0 3	9 0.9	6.0	2.0	7 0.4	0.4	2.0 4	9 0.4	5.0 13	3.0 9	9 0.	0.	6.0 6.0	M	.0 3.0	7.3
3.0 7.0 12.0 11.0 11.0 10.0 12.0 13.0 15	.0 11.0 11.0 10.0 12.0 13.0	11.0 10.0 12.0 13.0	.0 10.0 12.0 13.0	.0 12.0 13.0	.0 13.0	0.	1.0	.0 15	-	8.0 20	0.	18.0 20	0.0 2	1.0 16	5.0 14	4.0 14	4.0 12	.0 13	11 0.	.0 11.	.0 11.0	0.6 0	13.2
10.0 13.0 14.0 18.0 19.0 19.0 19.0 17.0 15	18.0 19.0 19.0 19.0 17.0	19.0 19.0 19.0 17.0	.0 19.0 19.0 17.0	.0 19.0 17.0	.0 17.0	.0 15		.0 17	7.0 18	.01	5.0 1	19.0 2	3.0 20	0.0 17	7.0 16	5.0 16	5.0 16	.0 16	8 0.0	.0 10	.0 17.0	0.91 0	16.2
12.0 15.0 14.0 13.0 12.0 13.0 13.0 15.0 15	13.0 12.0 13.0 13.0 15.0	12.0 13.0 13.0 15.0	.0 13.0 13.0 15.0	.0 13.0 15.0	15.0	0		.0 17	7.0 19	0	17.0 1	16.0 1	4.0 16	6.0 17	7.0 16	5.0 15	5.0 12	.0 10	0.0	.0 16	.0 15.	0 16.0	14.6
15.0 14.0 14.0 11.0 11.0 14.0 11.0 15.0 13	.0 11.0 11.0 14.0 11.0 15.0	11.0 14.0 11.0 15.0	.0 14.0 11.0 15.0	.0 11.0 15.0	15.0	0	20	.0 16	5.0 20	0	18.0 2	20.01	8.0 18	8.0 17	7.0 14	1.0 1	1.0 10	0.0 10	8 0.0	6 0.	.0 15.	0 14.0	14.0
17.0 18.0 14.0 12.0 17.0 17.0 18.0 16.0 1	.0 12.0 17.0 17.0 18.0 16.0	17.0 17.0 18.0 16.0	.0 17.0 18.0 16.0	.0 18.0 16.0	0.91 0.	0.	16	0.0	5.0 16	5.0 14	4.0 1	4.0 1	1.0 10	0.0	9.0 15	5.0 14	4.0 10	1.0 13	5.0 13	.0 11.	.0 13.	0 11.0	14.0
10.0 9.9 10.0 10.0 10.2 10.5 10.8 11.7 12	10.0 10.2 10.5 10.8 11.7	10.2 10.5 10.8 11.7	.2 10.5 10.8 11.7	.5 10.8 11.7	11.7	1.	(7)	.3 1	2.5 12	.7.1	2.6 1	3.2 1	3.5 13	3.3 13	3.5 13	3.4 12	2.9 11	.4 11	.6 10	.9 10	-4 10.	3 10.2	
# of Valid Hours = 638 % Data	= 638	= 638			% Dat	% Dat	4 .	ဒ္ဓ	mplete	eteness	<b>8</b> 0	85.8											





Envircon

Livingston, Montana

1ST QT '91

\*\*\* WIND FREQUENCY SUMMARY \*\*\*

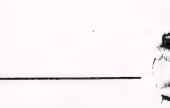
DIR>	2	NE	¥	ENE	ш	ESE	SE	SSE	S	MSS	AS.	MSM	3	285	3	N. C.	TOTAL
SPEED																	
(MPH)																	
0.0 - 4.0	1.4	2.3	1.0	7.0	7.0	7.0	0.0	0.5	0.3	6.0	0.7	7.0	9.0	0.2	8.0	1.0	10.7
4.0 - 7.5	1.1	1.4	9.0	9.0	0.1	0.5	0.0	0.0	0.1	0.5	1.5	1.9	8.0	7.0	7.0	9.0	10.1
7.5 - 12.1	1.4	1.1	0.1	1.4	0.3	0.1	0.0	0.0	0.1	1.8	7.4	7.8	2.7	7.0	0.2	8.0	25.5
	8.0	0.1	0.1	1.2	7.0	0.0	0.0	0.0	0.0	4.4	11.5	7.6	8.9	0.2	0.2	0.2	35.4
19.0 - 24.7	0.0	0.0	0.0	9.0	8.0	0.0	0.0	0.0	0.0	3.3	5.9	1.7	1.4	0.0	0.0	0.0	13.6
24.7 - 30.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.8	1.8	7.0	0.0	0.0	0.0	0.0	4.3
30.0 - 40.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.1	0.0	0.0	0.0	7.0
40.0 - 50.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
OVER 50.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL	4.5	6-7	1.7	4.1	2.2	7.0	0.0	0.2	0.5	12.7	28.8	22.2	12.2	1.2	1.5	2.5	
AVG. SPEED	7.5	5.4	1.5	11.9	14.4	4.7	0.0	1.5	8.4	17.0	15.3	13.4	14.4	8.0	6.3	2.9	
8	6			Ta+oT	Total Hours With Both Green and Direction =	ti tog	Speed			= 1037			A	ap ciu	Average Uind Speed	- 13.2	(MDH)
				10.0				2									
Resultant Windspeed	peedsp	6	9.3(MPH)		Resultant Wind		Direction =		236.00eg				Wind	Persis	Wind Persistance =	70.4	×



### JANUARY 1991

## \*\*\* WIND FREQUENCY SUMMARY \*\*\*

DIR>	2	NNE	NE.	ENE	ш	ESE	SE	SSE	s	MSS	MS	MSM	3	ZNZ	3	ZZZ	TOTAL
SPEED																	
0.0 - 4.0	0.8		0.3		0.0	0.5	0.0	0.3	0.0	0.0	0.5	0.5	0.5	0.0	0.3	0.0	7.0
	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.0	0.8	1.8	0.0	0.3	0.3	1.0	4.5
7.5 - 12.1	1.3		0.3		0.0	0.0	0.0	0.0	0.0	0.0	7.8	8.8	0.5	0.5	0.5	0.5	21.6
	2.0		0.0		0.5	0.0	0.0	0.0	0.0	2.0	18.3	11.3	3.5	0.0	0.0	0.5	40.1
19.0 - 24.7	0.0		0.0	0.0	1.3	0.0	0.0	0.0	0.0	3.3	9.5	4.0	1.5	0.0	0.0	0.0	19.5
24.7 - 30.0	0.0		0.0		0.0	0.0	0.0	0.0	0.0	3.3	4.3	1.8	0.0	0.0	0.0	0.0	9.3
	0.0		0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	8.0	0.3	0.0	0.0	0.0	1.0
40.0 - 50.0	0.0		0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
OVER 50.0	0.0		0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL	4.3	2.3	0.5	1.8	8.	0.5	0.0	0.3	0.3	8.5	41.1	28.8	6.3	0.8	1.0	2.0	
AVG. SPEED	10.6	7.6	6.0	15.9	19.9	4.0	0.0	2.0	5.0	22.7	16.9	14.8	16.5	8.0	7.3	8.9	
Calm Hours = 0.0%			To	Total Hours With Both Speed and Direction =	s With	Both Sp	eed and	l Direct		399		<	verage	Average Wind Speed =		15.9 (MPH)	<b>⊋</b>
Besultant Uindspeed	11	12.5 (MPH)	MPH)	Result	ant Win	Resultant Wind Direction =	tion =	233.9 Deg	Ded			3	ind Per	Wind Persistance =		78.6 %	





## FEBRUARY 1991

\*\*\* WIND FREQUENCY SUMMARY \*\*\*

D1R>	2	N.E.	¥	ENE	ш	ESE	SE	SSE		S	MSS	MS	MSM	3	ZNS	3		THE	TOTAL
SPEED																			
(MPH)																			
0.0 - 4.0	7.0	4.0	0.7	0.3	0			1.1	0.3	0.3	7.0	0.3	0.7	0		9.	0.1	9.0	8.9
	7.0	0.1	7.0	0.7	0			1.1	0.1	0.0	1.3	2.8	1.5	0		9.	7.0	0.3	10.9
	0.1	0.3	0.0	0.3	0.			0.0	0.0	0.0	1.3	5.8	13.2	3		.7	0.3	7.0	25.9
	9.0	0.0	0.0	7.0	0.			0.0	0.0	0.0	5.2	13.5	10.9	6.		٤,	7.0	0.3	38.1
	0.3	0.0	0.0	1.0	0			0.0	0.0	0.0	3.9	5.8	1.9	0		0.	0.0	0.0	13.2
24.7 - 30.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	1.3	3.6	0.0	0.0		0.0	0.0	0.0	6.4
	0.0	0.0	0.0	0.0	0			0.0	0.0	0.0	0.1	0.0	0.0	0		0.	0.0	0.0	0.1
	0.0	0.0	0.0	0.0	0			0.0	0.0	0.0	0.0	0.0	0.0	0		0.	0.0	0.0	0.0
ш 1	0.0	0.0	0.0	0.0	0.			0.0	0.0	0.0	0.0	0.0	0.0	0		0.	0.0	0.0	0.0
TOTAL	2.2	0.9	1.5	2.8	0.0	9.0 6		0.3	7.0	0.3	14.0	31.8	28.3	10.9		2.2	1.3	1.6	
AVG. SPEED	9.8	5.0	7.7	13.2	5.3	3 4.0		4.5	3.7	3.5	16.6	16.0	12.4	13.3		7.5	9.1	7.5	
			•	:				-			£						1 43	, munt	
Calm Hours = 0.0%			101	tal Hour	S WIT	Total Hours With Both Speed and Direction =	Speed	and u	recti		7/9			Verag	e Wind	Speed	2	Average wind speed = 15.0 (MPH)	

Wind Persistance = 81.2 %

Resultant Windspeed = 11.1 (MPH) Resultant Wind Direction = 234.4 Deg





### **MARCH 1991**

***	
RV	
CTIMMARV	
NU	֓֡֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֜֜֜֜֜֜֜֜֜֓֓֓֓֓֜֜֜֜֜֜֜֜
OTTE	
FRECIENCY	
UNLM	
***	

DIR>	Z	N. N.	믶		ENE	ш	ESE	SE	SSE	S	MSS	MS	MSM	3	TAN	3	322	TOTAL
SPEED																		
(MPH)																		
0.0 - 4.0			3.4	1.4	9.0	9.0	0.3	0.0	0.2					9.0	0.3	1.1	1.6	14.9
4.0 - 7.5		1.6 2	2.4	6.0	6.0	0.2	0.3	0.0	0.0					1.3	0.5	0.5	0.3	13.6
7.5 - 12.1	•		8.0	0.0	2.2	0.5	0.2	0.0	0.0	0.2	3.0	7.2		4.1	0.3	0.0	6.0	27.9
12.1 - 19.0			0.0	0.2	8.0	8.0	0.0	0.0	0.0					8.8	0.3	0.3	0.0	32.4
			0.0	0.0	6.0	0.5	0.0	0.0	0.0					1.3	0.0	0.0	0.0	6.6
24.7 - 30.0			0.0	0.0	0.0	0.0	0.0	0.0	0.0					0.0	0.0	0.0	0.0	1.3
		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				0.0	0.0	0.0	0.0	0.0	0.0
40.0 - 50.0			0.0	0.0	0.0	0.0	0.0	0.0	0.0					0.0	0.0	0.0	0.0	0.0
OVER 50.0			0.0	0.0	0.0	0.0	0.0	0.0	0.0				0.0	0.0	0.0	0.0	0.0	0.0
TOTAL	•	4.7 6	9.9	2.5	5.5	2.5	0.8	0.0	0.2	9.0	15.4	21.2	18.0	16.0	1.4	1.9	2.8	
AVG. SPEED	_,	5.8 4	4.5	6.4	11.1	12.0	5.0	0.0	1.0	4.8	15.0	13.4	12.0	13.8	8.0	0.9	5.7	
Calm Hours = 0	x0.0			Total	Hours	With	Total Hours With Both Speed and Direction =	eed and	Direc	tion =	638			lverage	Average Wind Speed = 11.6	eed = 1	11.6 (MPH)	£
			,							3				lind Day	4		¥	
Resultant Windspeed			(HPH) 4"/		(esnit	BUT WILL	Resultant Wind Direction =	TION =	738.2 Deg	nea				IIID LCI	WIND Persistance =		00°0	





## JANUARY 1991

## JANOARY

## \* \* \* WIND DIRECTION SUMMARY \* \* \*

DAY		C	•		L		1	c		9	HO	HOURS		;	<u>.</u>	·	•	0	ć				2	A	AVG
	<del></del>	7	m	4	5	9	_	œ	0	10		12	13	14	<u>.</u>	9	_		9 20	21	72	23	54		
-	•	•						•	•		,					,		,							•
2	•	•	•	•	,		,		,		•		•				ı								•
м	ŭ	•	•	•			,		,	,			٠	•			,						•		•
4	•						•											1					•		6
2	•		•	•	•	,	•		,	•						,		•					•		•
9	•	•				•	•		,	•	•				•	,							•		
7	•	•	1	•	•	•	•		•	•						•		•					•		•
80	٠		•						•			•								•			'		١
6	•	•	•	•				1	•		,		•						•				•		١
10	•	•					•	•						•									•		٠,
11	•	ı	•		•				,				•				,						•		•
12	•	•	•	٠			•	•							•		6						'		•
13	•	•	•											•	•							•	'		•
14	•	•	•	•		•	•					•								•	•				•
15	•	•	•	•				•	•	227	217			253								25 257			5
16	566	253	253	263			238																		2.8
17	238	240	225	228			525																		7
18	225	243	250	546			221																		7.2
19	217	344	359	0			357																		8.0
20	234	232	248	250			232																		9
21	238	238	240	237			232																		8
22	212	218	221	230		220	221																		-
23	331	308	22	~			332																		5.
54	253	220	210	219			226																		7.
25	216	221	M	19			324																		9
56	226	237	235	255	239		235																		6.3
27	260	544	255	564	258	274	274		569																4.0
28	332	8	88	9	29	92	29		89	88															9.
53	227	223	234	228	222	225	223	221	221	220	-														2.7
30	218	232	235	235	233	553	233	224	223	232		252		242	248	242 2	241 2	239 2	238 20	209 19	199 210		0 219		122.0
31	220	220	213	205	210	213	214	216	219	500	211		213	_									_		4
		*	of Valid Hours	id Ho	Urs =	398	~	% De	% Data Compl		eteness	11	3.5												





### FEBRUARY 1991

# \*\*\* WIND DIRECTION SUMMARY \*\*\*

### HOURS

DAY





### **MARCH 1991**

# \*\*\* WIND DIRECTION SUMMARY \*\*\*

HOURS

,		,	,	1		,							,	,		•			8		ć	Č	7	AVG.
7 8	7 8	7 8	7 8	7 8	7 8	7 8 9 10	8 9 10	9 10	0	-	-	2 1	3 1	4 15	,			15	50		22	23	54	
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				•	•		1	1													'	'		•
		1	1		•	1	1																	2.692
261 260 261 241 233 227 221	260 261 241 233 227 221	261 241 233 227 221	241 233 227 221	233 227 221	227 221	221		12	2															257.9
272 260 261 256 249 238 228 230 224	261 256 249 238 228 230	256 249 238 228 230	249 238 228 230	238 228 230	228 230	230		54	2	226 2	222	226 2		263 256		234 25	524 526	217	7 218	8 210	0 232	205	214	239.6
236 233 253 215 297 260 278	233 253 215 297 260 278	253 215 297 260 278	215 297 260 278	297 260 278	260 278	278		84	2				-											233.2
216 213 212 212 221 223 223	213 212 212 221 223 223	212 212 221 223 223	212 221 223 223	221 223 223	223 223	223		25	2															218.5
208 211 213 203 216 206 205	211 213 203 216 206 205	213 203 216 206 205	203 216 206 205	216 206 205	206 205	205		90	2															208.1
122 93 78 355 2 34 4	93 78 355 2 34 4	78 355 2 34 4	355 2 34 4	2 34 4	34 4	4		21																259.2
267 198 212 234 189 204 218 209	198 212 234 189 204 218 209	212 234 189 204 218 209	234 189 204 218 209	189 204 218 209	204 218 209	218 209	500		2															290.5
216 233 213 220 215 207 222 217	233 213 220 215 207 222 217	213 220 215 207 222 217	220 215 207 222 217	215 207 222 217	207 222 217	222 217	217		2															337.7
14 32 26 164 15 222 19 25	32 26 164 15 222 19 25	26 164 15 222 19 25	164 15 222 19 25	15 222 19 25	222 19 25	19 25	25																	344.5
226 293 215 233 231 225 237 228	293 215 233 231 225 237 228	215 233 231 225 237 228	233 231 225 237 228	231 225 237 228	225 237 228	237 228	228		2															341.9
54 19 20 26 348 26 349	19 20 26 348 26 349	20 26 348 26 349	26 348 26 349	348 26 349	26 349	349		88																334.6
249 242 246 266 44 44 212	242 246 266 44 44 212	246 266 44 44 212	266 44 44 212	44 44 212	44 212	212		14	2															346.4
240 242 237 225 215 201 198	242 237 225 215 201 198	237 225 215 201 198	225 215 201 198	215 201 198	201 198	198		03	2															206.1
28 29 8 25 9 31 31	29 8 25 9 31 31	8 25 9 31 31	25 9 31 31	9 31 31	31 31	31		43			_													52.2
198 250 229 234 234 230 237	250 229 234 234 230 237	229 234 234 230 237	234 234 230 237	234 230 237	230 237	237		20	2															218.4
227 234 219 225 215 220 221	234 219 225 215 220 221	219 225 215 220 221	225 215 220 221	215 220 221	220 221	221		13	2								-							229.7
258 253 245 259 270 277 283	253 245 259 270 277 283	245 259 270 277 283	259 270 277 283	270 277 283	277 283	283		92	7															266.7
243 232 236 250 239 237 258	232 236 250 239 237 258	236 250 239 237 258	250 239 237 258	239 237 258	237 258	258		41	7															43.9
79 74 88 88 34 69 24	74 88 88 34 69 24	88 88 34 69 24	88 34 69 24	34 69 24	69 24	54		9																74.5
31 320 215 340 358 239 61	320 215 340 358 239 61	215 340 358 239 61	340 358 239 61	358 239 61	239 61	61		38																75.5
78 63 336 356 343 341 354	63 336 356 343 341 354	336 356 343 341 354	356 343 341 354	343 341 354	341 354	354		5																71.9
281 242 236 231 245 272 278	242 236 231 245 272 278	236 231 245 272 278	231 245 272 278	245 272 278	272 278	278		91	2															268.3
261 255 270 279 272 281 272	255 270 279 272 281 272	270 279 272 281 272	279 272 281 272	272 281 272	281 272	272		63	2															269.8
254 252 250 251 257 257 265	. 252 250 251 257 257 265	250 251 257 257 265	251 257 255 265	257 257 265	257 265	592		62	2															259.6
250 250 236 233 218 230 217	250 236 233 218 230 217	236 233 218 230 217	233 218 230 217	218 230 217	230 217	217		10	2															261.8
219 229 224 217 216 202 205	229 224 217 216 202 205	224 217 216 202 205	217 216 202 205	216 202 205	202 202	202		05	7	04 2			210 20											211.5
# of Valid Hours = 638 % Data Comp	Valid Hours ≈ 638	Valid Hours ≈ 638	<b>=</b> 638	<b>=</b> 638	638 % Data Co	% Data Co	% Data Co	в Со	=	olet	eness	<b>=</b> 85	89											





Envirocon \*\*\* WIND SIGMA SUMMARY (DEGREES) \*\*\*

AVG.		0	0	0	0	0	0	0	0	0	0	0	0	0	0	16	17	14	14	20	12	12	19	52	22	92	12	13	19	5	16	5	
~	54				•		1	,						,	•	11	16	17	12	15	10	13	14	17	80	12	7	18	10	23	17	15	8
	23		,					,	,					,		10	13	13	10	15	13	13	2	16	15	15	7	14	14	23	17	13	18
	22				•		•				•			,		18	11	16	11	14	10	17	41	20	95	45	10	15	29	21	18	17	23
	21			,		•	•	•		•	•			•	•	20	15	15	12	12	12	16	97	12	17	1	10	18	69	54	14	14	19
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Envirocon \*\*\* WIND SIGMA SUMMARY (DEGREES) \*\*\*

HOURS

AVG.		15	12	16	15	18	43	13	50	27	50	15	16	13	25	15	23	15	14	16	14	19	59	32	33	52	16	23	15	0	0	0	
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Envirocon \*\*\* WIND SIGMA SUMMARY (DEGREES) \*\*\*

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Envirocon \*\*\* TEMPERATURE SUMMARY (DEG F) \*\*\*

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Envirocon \*\*\* TEMPERATURE SUMMARY (DEG F) \*\*\*

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	23	48	94	43	45	39	37	94	41	32	37	48	39	39	43	48	36	34	32	48	20	34	34	30	36	30	28	36	12				38	
	22	48	95	43	94	43	30	94	41	34	41	20	39	39	43	48	34	32	32	94	20	36	36	36	36	30	30	37	12	•	1		39	
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	19	20	20	94	94	95	37	20	95	45	45	52	39	41	41	52	37	34	34	94	48	95	94	39	34	36	39	39	18	ı	•	ı	45	
	18	20	52	48	48	48	43	54	20	52	20	24	41	41	43	54	41	36	36	94	20	48	20	43	36	39	45	41	18		,	1	45	
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RAILYARD

\*\*\* TEMPERATURE SUMMARY (DEG F) \*\*\*

HOURS

DAY

AVG.		0	0	0	0	82	52	30	34	41	45	31	32	38	31	*	32	34	17	75	43	38	39	38	37	×	52	33	37	36	75	52		
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	23	,	•	,	•	23	52	28	36	45	36	52	32	30	30	30	30	34	39	41	37	37	39	34	39	28	23	%	34	39	94	52	34	
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### APPENDIX B QUALITY ASSURANCE/QUALITY CONTROL



### CERTIFICATION OF DATA INTEGRITY

Bison Engineering Inc. certifies that the data contained herein are, to the best of our knowledge, an accurate summary of air quality and meteorological conditions measured at the Livingston Railyard in Livingston, MT. Every effort was made to obtain accurate and representative data and to comply with procedures set forth in the Quality Assurance Handbook for Air Pollution Measurement Systems; Volume II, Ambient Air Specific Methods (EPA-600/4-77-027a) and the conditions of Section 14.4 of the Interim Remedial Measures Work Plan (work plan) as required by the Montana Department of Health and Environmental Sciences.

Project Manager: Hawle W Roll

Title: Vice President

Date: February 28, 1991





### BISON ENGINEERING INC Helena, Montana

PM-10 Calibration - Wedding Assoc.

Calibrated	by Scott F and Dan M	Location Livingston
Date Man	rch 29, 1991	Sampler # Upwind - #3
Look-up :		
	20" U-Tube Manometer:	" Water = delta
	Barometric Pressure:	" Mercury = P0
	Temperature:	40 F
	P1/P0 = 0.939	{P1=P0 - delta/13.6
	Look-up = 39.173	= Look-ACFM
	Look-SCFM = 35.578	(std ft^3/min)
	= ACFM[P0*298]	]/29.92*Tk] Tk=temp degrees K
Orifice:		
	10 " Manometer 4.3	" (Clean Filter)
	Q = .49134	.49610 (dP)
	= 1.013	3 (m^3/min)
	Qcfm = Q*35.314	
	= 35.776	(acfm)r
	Qscfm = Qcfm[(P0*29	0.5 98)/(29.92*Tk)]
	= 34.095	
% Diffe	rence: 4.4	_ %
Adjustm	ent: N/A	_ (if necessary)

Clean Filter Transducer:



### BISON ENGINEERING INC Helena, Montana

PM-10 Calibration - Wedding Assoc.

Calibrated	by Scott F	and Dan M	Location _	Livingston	
Date Ma	rch 29, 1991		Sampler #	Downwind #4	
Look-up :					
	20" U-Tube M	fanometer:	21.3	" Water = delt	:a
	Barometric F	ressure :	25.3 "	" Mercury = PO	
	Temperature:		40 F		
	P1/P0 = 0.	938	{P1=P0 -	delta/13.6	
	$Look-up = _3$	88.825	= Look-A	CFM	
	Look-SCFM =	35.262	(st	d ft^3/min)	
	= 2	CFM[P0*298]	/29.92*Tk]	Tk=temp degrees H	<
Orifice:					
	10 " Manome	eter <u>4.1</u>		(Clean Filter)	
		Q = .49134	.49610 (dP)		
		= 1.001	(m	^3/min)	
	Qcfm = Q	2*35.314			
	=	35.361	_ (acfm)r		
	Qscfm =	Qcfm[(P0*29	8)/(29.92*T	0.5 k)]	
	=	33.699			
% Diffe	rence:	1.6	ફ		
Adjustm	ent: 1	N/A	(if n	ecessary)	17.

Clean Filter Transducer:



Helena, Montana

PM-10 Auditing - Wedding Assoc.

Audited by Scott Fitzpatrick Location Livingston Date March 29, 1991 Sampler # Upwind #3 Look-up: P1/P0 = 0.939 (from previous calibration) Temperature: 40 F (degrees K)

Look-up = 39.173 = Look-ACFM

 $Look-SCFM = 35.135 (std ft^3/min)$ = ACFM[P0\*298]/29.92\*Tk] Tk=temp degrees K

Audit Orifice

10 " Manometer 2.7 " (Clean Filter) Q = .62283 (dP)

 $= 1.010 (m^3/min)$ 

Qcfm = Q\*35.314

= 35.658 (acfm)r

Qscfm = Qcfm[(P0\*298)/(29.92\*Tk)]

= 33.881

-0.5Qacfm = Qcfm[(P0\*298)/(29.92\*Tk)]Clean Filter Trans. ---

% Difference: 3.7 % (from SCFM)

% Difference: -6.7 % (from 40 ACFM)



Helena, Montana

PM-10 Auditing - Wedding Assoc.

Audited by Scott Fitzpatrick Location Livingston

Date March 29, 1991 Sampler # Downwind #4

Look-up:

P1/P0 = 0.938 (from previous calibration)

Temperature: 40 F (degrees K)

Look-up = 38.825 = Look-ACFM

 $Look-SCFM = 35.052 (std ft^3/min)$ 

= ACFM[P0\*298]/29.92\*Tk] Tk=temp degrees K

Audit Orifice

10 " Manometer 2.7 " (Clean Filter)

.48645

Q = .62283 (dP)

= 1.010 (m<sup>3</sup>/min)

Qcfm = Q\*35.314

= 35.658 (acfm)r

Qscfm = Qcfm[(F0\*298)/(29.92\*Tk)]

= 33.881

Qacfm = Qcfm[(P0\*298)/(29.92\*Tk)] = 37.528

Clean Filter Trans. \_\_\_\_

% Difference: 3.5 % (from SCFM)

% Difference: \_-6.7 % (from 40 ACFM)



Helena, Montana

### Total Suspended Particulate - Calibration Envirocon

Calibrated by Scott F and Dan M Location Livingston

Date March 29, 1991 Sampler # Downwind #4

.49610

Calibration Equation: Qr = .49134 (dP)

Run	Plate No.	P1 (left)	P2 (right)	dP (total)	TR	dr *	qr +
1	18	4.2	4.1	8.3	45	1.404	1.387
2	13	3.0	2.9	5.9	38	1.185	1.189
3	10	2.7	2.7	5.4	36	1.134	1.129
4	7	1.8	1.8	3.6	30	0.928	0.951
5	5	1.1	1.1	2.2	22	0.727	0.713

Qr = flow rate by Orifice equation

Qr = flow rate from transducer regression equation

### Results--

$$Qr = a(TR) + b = 0.029747 (TR) + 0.05815$$





Helena, Montana

Total Suspended Particulate - Audit

Audited by	Scott Fitzpatrick	Company	Envirocon
Date 3/29/	91	Project	Livingston Railyard
		.486	45

Audit Equation: Qr = .62283 (dP)

Sample #	Plate No.	P1 (left)	P2 (right)	dP (total)	TR	Qr	Qr +
4	18	1.8	1.8	3.6	39	1.162	1.092
	18						
	18						
	18	-					
	18						

Qr = flow rate by Audit Equation

Qr = flow rate from previous calibration equation

Results:

Sampler #	% Difference	
_4_	<u>-5.9</u> %	
	* * * * * * * * * * * * * * * * * * *	



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